US007168185B2

(12) **United States Patent**
Ellis, III

(10) **Patent No.:** **US 7,168,185 B2**
(45) **Date of Patent:** *Jan. 30, 2007

(54) **SHOES SOLE STRUCTURES**

(75) Inventor: **Frampton E. Ellis, III**, Arlington, VA (US)

(73) Assignee: **Anatomic Research, Inc.**, Jasper, FL (US)

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 56 days.

This patent is subject to a terminal disclaimer.

(21) Appl. No.: **10/690,933**

(22) Filed: **Oct. 22, 2003**

(65) **Prior Publication Data**

US 2004/0134096 A1 Jul. 15, 2004

Related U.S. Application Data

(60) Division of application No. 09/974,786, filed on Oct. 12, 2001, now Pat. No. 6,729,046, which is a division of application No. 09/907,598, filed on Jul. 19, 2001, now Pat. No. 6,591,519, which is a division of application No. 09/734,905, filed on Dec. 13, 2000, now Pat. No. 6,308,439, which is a continuation of application No. 08/477,954, filed on Jun. 7, 1995, now Pat. No. 6,163,982, which is a continuation-in-part of application No. 08/376,661, filed on Jan. 23, 1995, now Pat. No. 6,810,606, which is a continuation of application No. 08/127,487, filed on Sep. 28, 1993, now abandoned, which is a continuation of application No. 07/729,886, filed on Jul. 11, 1991, now abandoned, which is a continuation of application No. 07/400,714, filed on Aug. 30, 1989, now abandoned.

(51) **Int. Cl.**
A43B 13/12 (2006.01)

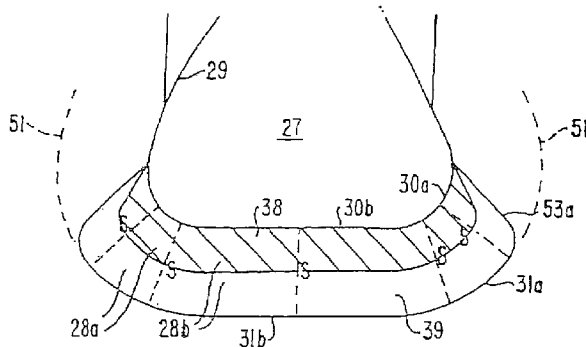(52) **U.S. Cl.** .... **36/25 R**; 36/88

(58) **Field of Classification Search** .... 36/25 R, 36/32 R, 30 R, 31, 14, 114, 15, 88, 89, 11, 36/12, 92, 127, 93, 91, 113, 115, 140, 143, 36/144
See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

119,894	A	10/1871	Smyth
193,914	A	8/1877	Berry
280,791	A	7/1883	Brooks
288,127	A	11/1883	Shepard
500,385	A	6/1893	Hall
532,429	A	1/1895	Rogers
584,373	A	6/1897	Kuhn
1,283,335	A	10/1918	Shillcock
1,289,106	A	12/1918	Bullock
D55,115	S	5/1920	Barney
1,458,446	A	6/1923	Shaefer
1,622,860	A	3/1927	Cutler
1,639,381	A	8/1927	Manelas
1,701,260	A	2/1929	Fischer
1,735,986	A	11/1929	Wray
1,853,034	A	4/1932	Bradley
1,870,751	A	8/1932	Reach
2,120,987	A	6/1938	Murray
2,124,986	A	7/1938	Pipes
2,147,197	A	2/1939	Glidden
2,155,166	A	4/1939	Kraft
2,162,912	A	6/1939	Craver
2,170,652	A	8/1939	Brennan
2,179,942	A	11/1939	Lyne
D119,894	S	4/1940	Sherman
2,201,300	A	5/1940	Prue
2,206,860	A	7/1940	Sperry
D122,131	S	8/1940	Sannar
D128,817	S	8/1941	Esterson
2,251,468	A	8/1941	Smith
2,328,242	A	8/1943	Witherill
2,345,831	A	4/1944	Pierson
2,433,329	A	12/1947	Adler et al.
2,434,770	A	1/1948	Lutey
2,470,200	A	5/1949	Wallach
2,627,676	A	2/1953	Hack
2,718,715	A	9/1955	Spilman
2,814,133	A	11/1957	Herbst
3,005,272	A	10/1961	Shelare

3,100,354 A	8/1963	Lombard et al.	
3,110,971 A	11/1963	Chang	
3,305,947 A	2/1967	Kalsoy	
3,308,560 A	3/1967	Jones	
3,416,174 A	12/1968	Novitske	
3,512,274 A	5/1970	McGrath	
3,535,799 A	10/1970	Onitsuka	
3,806,974 A	4/1974	Di Paolo	
3,824,716 A	7/1974	Di Paolo	
3,863,366 A	2/1975	Auberry et al.	
3,958,291 A	5/1976	Spier	
3,964,181 A	6/1976	Holcombe, Jr.	
3,997,984 A	12/1976	Hayward	
4,003,145 A	1/1977	Liebscher et al.	
4,030,213 A	6/1977	Daswick	
4,043,058 A	8/1977	Hollister et al.	
4,068,395 A	1/1978	Senter	
4,083,125 A	4/1978	Benseler et al.	
4,096,649 A	6/1978	Saurwein	
4,098,011 A	7/1978	Bowerman et al.	
4,128,950 A	12/1978	Bowerman et al.	
4,128,951 A	12/1978	Tansill	
4,141,158 A	2/1979	Benseler et al.	
4,145,785 A	3/1979	Lacey	
4,149,324 A	4/1979	Lesser et al.	
4,161,828 A	7/1979	Benseler et al.	
4,161,829 A	7/1979	Wayser	
4,170,078 A	10/1979	Moss	
4,183,156 A	1/1980	Rudy	
4,194,310 A	3/1980	Bowerman	
D256,180 S	8/1980	Turner	D2/309
D256,400 S	8/1980	Famolare, Jr.	D2/320
4,217,705 A	8/1980	Donzis	
4,219,945 A	9/1980	Rudy	
4,223,457 A	9/1980	Borgeas	
4,227,320 A	10/1980	Borgeas	
4,235,026 A	11/1980	Plagenhoef	
4,237,627 A	12/1980	Turner	
4,240,214 A	12/1980	Sigle et al.	
4,241,523 A	12/1980	Daswick	
4,245,406 A	1/1981	Landay et al.	
4,250,638 A	2/1981	Linnemann	
4,258,480 A	3/1981	Famolare, Jr.	
4,259,792 A	4/1981	Halberstadt	
4,262,433 A	4/1981	Hagg et al.	
4,263,728 A	4/1981	Frecentese	
4,266,349 A	5/1981	Schmohl	
4,268,980 A	5/1981	Gudas	
4,271,606 A	6/1981	Rudy	36/29
4,272,858 A	6/1981	Hlustik	
4,274,211 A	6/1981	Funck	
4,297,797 A	11/1981	Meyers	
4,302,892 A	12/1981	Adamik	
4,305,212 A	12/1981	Coomer	
4,308,671 A	1/1982	Bretschneider	
4,309,832 A	1/1982	Hunt	
4,314,413 A	2/1982	Dassier	36/36
4,316,332 A	2/1982	Giese et al.	
4,316,335 A	2/1982	Giese et al.	
4,319,412 A	3/1982	Muller et al.	
D264,017 S	4/1982	Turner	D2/310
4,322,895 A	4/1982	Hockerson	
D265,019 S	6/1982	Vermonet	
4,335,529 A	6/1982	Badalamenti	
4,340,626 A	7/1982	Rudy	
4,342,161 A	8/1982	Schmohl	
4,348,821 A	9/1982	Daswick	
4,354,319 A	10/1982	Block et al.	
4,361,971 A	12/1982	Bowerman	
4,364,188 A	12/1982	Turner et al.	
4,366,634 A	1/1983	Giese et al.	
4,370,817 A	2/1983	Ratanangsu	
4,372,059 A	2/1983	Ambrose	
4,398,357 A	8/1983	Batra	
4,399,620 A	8/1983	Funck	
D272,294 S	1/1984	Watanabe	
4,435,910 A	3/1984	Marc	
4,449,306 A	5/1984	Cavanagh	
4,451,994 A	6/1984	Fowler	
4,454,662 A	6/1984	Stubblefield	
4,455,765 A	6/1984	Sjosward	
4,455,767 A	6/1984	Bergmans	
4,468,870 A	9/1984	Sternberg	
4,484,397 A	11/1984	Curley, Jr.	
4,494,321 A	1/1985	Lawlor	
4,505,055 A	3/1985	Bergmans	
4,506,462 A	3/1985	Cavanagh	
4,521,979 A	6/1985	Blaser	
4,527,345 A	7/1985	Lopez Lopez	
D280,568 S	9/1985	Stubblefield	
4,542,598 A	9/1985	Misevich et al.	
4,546,559 A	10/1985	Dassler	
4,550,510 A	11/1985	Stubblefield	
4,557,059 A	12/1985	Misevich et al.	
4,559,723 A	12/1985	Hamy et al.	
4,559,724 A	12/1985	Norton	
4,561,195 A	12/1985	Onoda et al.	
4,577,417 A	3/1986	Cole	
4,578,882 A	4/1986	Talarico, II	
4,580,359 A	4/1986	Kurrash et al.	
4,624,061 A	11/1986	Wezel et al.	
4,624,062 A	11/1986	Autry	
4,641,438 A	2/1987	Laird et al.	
4,642,917 A	2/1987	Ungar	
4,651,445 A	3/1987	Hannibal	
D289,341 S	4/1987	Turner	
4,670,995 A	6/1987	Huang	
4,676,010 A	6/1987	Cheskin	
4,694,591 A	9/1987	Banich et al.	
4,697,361 A	10/1987	Ganter et al.	
D293,275 S	12/1987	Bua	
4,715,133 A	12/1987	Hartjes et al.	
4,722,677 A	2/1988	Rebers	
4,724,622 A	2/1988	Mills	
D294,425 S	3/1988	Le	
4,727,660 A	3/1988	Bernhard	
4,730,402 A	3/1988	Norton et al.	
4,731,939 A	3/1988	Parracho et al.	
4,747,220 A	5/1988	Autry et al.	
D296,149 S	6/1988	Diaz	
D296,152 S	6/1988	Selbiger	
4,748,753 A	6/1988	Ju	
4,754,561 A	7/1988	Dufour	
4,756,098 A	7/1988	Boggia	
4,757,620 A	7/1988	Tiltola	
4,759,136 A	7/1988	Stewart et al.	
4,768,295 A	9/1988	Ito	
4,769,926 A	9/1988	Meyers	
D298,684 S	11/1988	Pitchford	
4,785,557 A	11/1988	Kelley et al.	
4,817,304 A	4/1989	Parker et al.	
4,827,631 A	5/1989	Thornton	
4,833,795 A	5/1989	Diaz	
4,837,949 A	6/1989	Dufour	
D302,900 S	8/1989	Kolman et al.	
4,854,057 A	8/1989	Misevich et al.	
4,858,340 A	8/1989	Pasternak	
4,866,861 A	9/1989	Noone	
4,876,807 A	10/1989	Tiitola et al.	
4,890,398 A	1/1990	Thomasson	
4,894,933 A	1/1990	Tonkel et al.	
4,897,936 A	2/1990	Fuerst	
4,906,502 A	3/1990	Rudy	
4,918,841 A	4/1990	Turner et al.	
4,922,631 A	5/1990	Anderie	
4,934,070 A	6/1990	Mauger	

Patent No.		Date	Name			
4,934,073	A	6/1990	Robinson			
D310,131	S	8/1990	Hase			
D310,132	S	8/1990	Hase			
4,947,560	A	8/1990	Fuerst et al.			
4,949,476	A	8/1990	Anderie			
D310,906	S	10/1990	Hase			
4,982,737	A	1/1991	Guttmann			
4,989,349	A	2/1991	Ellis, III			
D315,634	S	3/1991	Yung-Mao			
5,010,662	A	4/1991	Dabuzhsky et al.			
5,014,449	A	5/1991	Richard et al.			
5,024,007	A	6/1991	DuFour			
5,025,573	A	6/1991	Giese et al.			
D320,302	S	10/1991	Kiyosawa			
5,052,130	A	10/1991	Barry et al.			
5,077,916	A	1/1992	Beneteau			
5,079,856	A	1/1992	Truelsen			
5,092,060	A	3/1992	Frachey et al.			
D327,164	S	6/1992	Hatfield			
D327,165	S	6/1992	Hatfield			
5,131,173	A	7/1992	Anderie			
D328,968	S	9/1992	Tinker			
D329,528	S	9/1992	Hatfield			
D329,739	S	9/1992	Hatfield			
D330,972	S	11/1992	Hatfield et al.			
D332,344	S	1/1993	Hatfield et al.			
D332,692	S	1/1993	Hatfield et al.			
5,191,727	A	3/1993	Barry et al.			
5,224,280	A	7/1993	Preman et al.			
5,224,810	A	7/1993	Pitkin			
5,237,758	A	8/1993	Zachman			
D347,105	S	5/1994	Johnson			
5,317,819	A	6/1994	Ellis, III			
5,369,896	A	12/1994	Frachey et al.			
D372,114	S	7/1996	Turner et al.			
5,543,194	A	8/1996	Rudy			
5,544,429	A	8/1996	Ellis, III			
5,572,805	A	11/1996	Giese et al.			
5,575,089	A	11/1996	Giese et al.			
5,628,128	A	5/1997	Miller et al.			
D388,594	S	1/1998	Turner et al.			
D409,362	S	5/1999	Turner et al.			
D409,826	S	5/1999	Turner et al.			
D410,138	S	5/1999	Turner et al.			
5,909,948	A	6/1999	Ellis, III			
6,115,941	A	9/2000	Ellis, III			
6,115,945	A	9/2000	Ellis, III			
6,163,982	A	12/2000	Ellis, III			
D444,293	S	7/2001	Turner et al.			
D450,916	S	11/2001	Turner et al.			
6,584,706	B1	7/2003	Ellis, III			
6,591,519	B1	7/2003	Ellis, III			
6,609,312	B1	8/2003	Ellis, III			
6,629,376	B1	10/2003	Ellis, III			
6,662,470	B2	12/2003	Ellis, III			
6,668,470	B2	12/2003	Ellis, III			
6,675,498	B1 *	1/2004	Ellis, III	.... 36/25 R		
6,675,499	B2	1/2004	Ellis, III			
6,708,424	B1	3/2004	Ellis, III			
6,729,046	B2 *	5/2004	Ellis, III	.... 36/25 R		
6,748,674	B2	6/2004	Ellis, III			
6,763,616	B2	7/2004	Ellis, III			
6,789,331	B1 *	9/2004	Ellis, III	.... 36/25 R		
6,810,606	B1	11/2004	Ellis, III			
6,877,254	B2	4/2005	Ellis, III			
6,918,197	B2	7/2005	Ellis, III			

FOREIGN PATENT DOCUMENTS

Country	No.	Date
AT	200963	5/1958
CA	1 138 194	12/1982
CA	1 176 458	10/1984
DE	B23257 VII/71 A	5/1957
DE	1 888 119	12/1963
DE	1918131	6/1965
DE	1918132	6/1965
DE	1 287 477	1/1969
DE	1 290 844	3/1969
DE	2036062	7/1970
DE	1948620	5/1971
DE	1685293	7/1971
DE	1 685 260	10/1971
DE	2045430	3/1972
DE	2522127	11/1976
DE	2525613	12/1976
DE	2602310	7/1977
DE	2613312	10/1977
DE	27 06 645	8/1978
DE	2654116	1/1979
DE	27 37 765	3/1979
DE	28 05 426	8/1979
DE	3021936	4/1981
DE	30 24 587 A1	1/1982
DE	8219616.8	9/1982
DE	3113295	10/1982
DE	32 45 182	5/1983
DE	33 17 462	10/1983
DE	831831.7	12/1984
DE	8431831	12/1984
DE	3347343	7/1985
DE	8530136.1	2/1988
DE	36 29 245	3/1988
EP	0 048 965	4/1982
EP	0 083 449 A1	7/1983
EP	0 130 816	1/1985
EP	0 185 781	7/1986
EP	0207063	10/1986
EP	0 206 511	12/1986
EP	0 213 257	3/1987
EP	0 215 974	4/1987
EP	0 238 995	9/1987
EP	0 260 777	3/1988
EP	0 301 331 A2	2/1989
EP	0 329 391	8/1989
EP	0 410 087 A2	1/1991
FR	602.501	3/1926
FR	925.961	9/1947
FR	1.004.472	3/1952
FR	1245672	10/1960
FR	1.323.455	2/1963
FR	2 006 270	11/1971
FR	2 261 721	9/1975
FR	2 511 850	3/1983
FR	2 622 411	5/1989
GB	16143	2/1892
GB	9591	11/1913
GB	764956	1/1957
GB	807305	1/1959
GB	1504615	3/1978
GB	2 023 405	1/1980
GB	2 039 717 A	8/1980
GB	2076633	12/1981
GB	2133668	8/1984
GB	2 136 670	9/1984
JP	39-15597	8/1964
JP	45-5154	3/1970
JP	50-71132	11/1975
JP	57-139333	8/1982
JP	59-23525	7/1984
JP	61-55810	4/1986
JP	1129505	6/1986
JP	61-167810	10/1986
JP	1-195803	8/1989
JP	2136505	5/1990
JP	2279103	11/1990
JP	3-85102	4/1991

JP	3086101	4/1991
JP	4-279102	10/1992
JP	5-123204	5/1993
NZ	189890	9/1981
WO	WO 87/07480	12/1987
WO	WO8707481	12/1987
WO	WO 88/08263	11/1988
WO	WO 89/06500	7/1989
WO	WO 90/00358	1/1990
WO	WO 91/00698	1/1991
WO	WO 91/03180	3/1991
WO	WO 91/04683	4/1991
WO	WO 91/05491	5/1991
WO	WO 91/10377	7/1991
WO	WO 91/11124	8/1991
WO	WO 91/11924	8/1991
WO	WO 91/19429	12/1991
WO	WO 92/07483	5/1992
WO	WO 92/18024	10/1992
WO	WO 93/13928	7/1993
WO	WO 94/03080	2/1994
WO	WO 97/00029	1/1997
WO	WO 00/64293	11/2000

OTHER PUBLICATIONS

Johnson et al., << A Biomechanicl Approach to the Design of Football Boots >>, *Journal of Biomechanics*, vol. 9, pp. 581-585 (1976).
Fixx, *The Complete Book of Running*, pp. 134-137 1977.
Romika Catalog, Summer 1978.
adidas shoe, Model << Water Competition >> 1980.
World Professional Squash Association Pro Tour Program, 1982-1983.
Williams et al., << The Mechanics of Foot Action During The GoldSwing and Implications for Shoe Design >>, *Medicine and Science in Sports and Exercise*, vol. 15, No. 3, pp. 247-255 1983.
Nigg et al., << Biomechanical Aspects of Sport Shoes and Playing Surfaces >>, *Proceedings of the International Symposium on Biomechanical Aspects of Sport Shoes and Playing Surfaces*, 1983.
Valiant et al., << A Study of Landing from a Jump : Implications for the Design of a Basketball Shoe >>, *Scientific Program of IX Internatioanl Congress of Biomechanics*, 1983.
Frederick, *Sports Shoes and Playing Surfaces, Biomechanical Properties*, Entire Book, 1984.
Saucony Spot-bilt Catalog Supplement, Spring 1985.
adidas shoe, Model << Fire >> 1985.
adidas shoe, Model "Tolio H. ", 1985.
adidas shoe, Model "Buffalo " 1985.
adidas shoe, Model "Marathon " 86 1985.
adidas shoe, Model << Boston Super >> 1985.
Leuthi et al., << Influence of Shoe Construction on Lower Extremity Kinematics and Load During Lateral Movements In Tennis <<, *International Journal of Sports Biomechanics*, , vol. 2, pp. 166-174 1986.
Nigg et al., *Biomechanics of Running Shoes*, entire book, 1986.
Runner's World, Oct. 1986.
AVIA Catalog 1986.
Brooks Catalog 1986.
adidas Catalog 1986.
adidas shoe, Model << Questar >>; 1986.
adidas shoe, Model "London" 1986.
adidas shoe, Model << Marathon >> 1986.
adidas shoe, Model << Tauern >> 1986.
adidas shoe, Model << Kingscup Indoor >>, 1986.
Komi et al., "Interaction Between Man and Shoe in Running: Considerations for More Comprehensive Measurement Approach", *International Journal of Sports Medicine*, vol. 8, pp. 196-202 1987.
Nigg et al., << The Influence of Lateral Heel Flare of Running Shoes on Protraction and Impact Forces >>, *Medicine and Science in Sports and Excercise*, vol. 19, No. 3, pp. 294-302 1987.
Nigg, << Biomechanical Analysis of Ankle and foot Movement >> *Medicine and Sport Science*, vol. 23, pp. 22-29 1987.

Saucony Spot-bilt shoe, *The Complete Handbook of Athletic Footwear*, pp. 332, 1987.
Puma basketball shoe, *The Complete Handbook of Athletic Footwear*. pp. 315, 1987.
addidas shoe, Model, << Indoor Pro >> 1987.
adidas Catalog, 1987.
adidas Catalog, Spring 1987.
Nike Fall Catalog 1987, pp. 50-51.
Footwear Journal, Nike Advertisement, Aug. 1987.
Sporting Goods Business, Aug. 1987.
Nigg et al., "Influence of Hell Flare and Midsole Construction on Pronation" *International Journal of Sport Biomechanics*, vol. 4, No. 3, pp. 205-219, (1987).
Vagenas et al., << Evaluationm of Rearfoot Asymmetrics in Running With Worn and New Running Shoes << , *International Journal of Sport Biomechanics*, vol. 4, No. 4, pp. 342-357 (1988).
Fineagan, "Comparison of the Effects of a Running Shoe and A Racing Flat on the Lower Extremity Biomechanical Alignment of Runners", *Journal of the American Physical Therapy Association*, vol. 68, No. 5, p. 806 (1988).
Nawoczenside et al., << Effect of Rocker Sole Design on Plantar Forefoot Pressures >> *Journal of the American Podiatric Medical Association*, vol. 79, No. 9, pp. 455-460, 1988.
Sprts Illustrated, Special Preview Issue, The Summer Olympics << Seoul '88 >> Reebok Advertistement.
Sports Illustrated, Nike Advertisement, Aug. 8, 1988.
Runner's World, "Shoe Review" Nov. 1988 pp. 46-74.
Footwear Nows, Special Supplement, Feb. 8, 1988.
Footwear New, vol. 44, No. 37, Nike Advertisement (1988).
Saucony Spot-bilt Catalog 1988.
Runner's World, Apr. 1988.
Footwear News, Special Supplement, Feb. 8, 1988.
Kronos Catalog, 1988.
Avia Fall Catalog 1988.
Nike shoe, Model << High Jump 88 >>, 1988.
Nike shoe, Model << Zoom Street Leather >> 1988.
Nike shoe, Model << Leather Cortex® >>, 1988.
Nike shoe, Model << Air Revolution >> #15075, 1988.
Nike shoe, Model "Air Force " #1978, 1988.
Nike shoe, Model << Air Flow << #718,1988.
Nike shoe, Model "Air" #1553, 1988.
Nike shoe, Model << Air >>, #13213 1988.
Nike shoe, Model << Air >>, #4183, 1988.
Nike Catalog, Footwear Fall, 1988.
adidas shoe Model "Skin Racer" 1988.
adidas shoe, Model <<Tennis Comfort >> 1988.
adidas Catalog 1988.
Segesser et al., "Surfing Shoe", *The Shoe in Sport*, 1989, (Translation of a book published in Germany in 1987), pp. 106-110.
Palamarchuk et al., "In shoe Casting Technique for Specialized Sports Shoes", *Journal of the America Podiatric Medical Association*, vol. 79, No. 9, pp. 462-465 1989.
Runner's World, "Spring Shoe Survey", pp. 45-74.
Footwear News, vol. 45, No. 5, Nike Advertisement 1989.
Nike Spring Catalog 1989 pp. 62-63.
Prince Cross-Sport 1989.
adidas Catalog 1989.
adidas Spring 1989.
adidas Autumn Catalog 1989.
Nike Shoe, men's cross-training Model "Air Trainer SC" 1989.
Nike shoe, men's cross-training Model << Air Trainer TW >> 1989.
adidas shoe, Model "Torsion Grand Slam Indoor", 1989.
adidas shoe, Model << Torsion ZC 9020 S >> 1989.
adidas shoe, Model << Torison Special HI >> 1989.
Areblad et al., << Three-Dimensional Measurement of Rearfoot Motion During Running >> *Journal of Biomechanics*, vol. 23, pp. 933-940 (1990).
Cavanagh et al., "Biomechanics of Distance Running", Human Kinetics Books, pp. 155-164 1990.
adidas Catalog 1990.
adidas Catalog 1991.
K-Swiss Catalog, Fall 1991.

Originally filed specification for U.S. Appl. No. 09/785,200, filed Feb. 20, 2001 (ELL-012D/Div 2).

Originally filed specification for U.S. Appl. No. 09/734,905, filed Dec. 13, 2000 (ELL-012D/Div 1).

Originally filed specification for U.S. Appl. No. 09/790,626, filed Feb. 23, 2001 (ELL-003/Div 3).

Originally filed specification for U.S. Appl. No. 09/780,450, filed Feb. 12, 2001 (ELL-003/Div 2).

Originally filed specification for U.S. Appl. No. 09/710,952, filed Nov. 14, 2000 (ELL-003/Div 1).

Originally filed specification for U.S. Appl. No. 08/376,661, filed Jan. 23, 1995 (ELL-003/FWCon3).

Originally filed specification for U.S. Appl. No. 08/482,838, filed Jun. 7, 1995 (ELL-011).

Originally filed specification for U.S. Appl. No. 08/462,490, filed May 30, 1995 (ELL-004/Con3) and Originally filed specification for U.S. Appl. No. 08/473,974, filed Jun. 7, 1995 (ELL-012M).

Originally filed specification for U.S. Appl. No. 08/479,776, filed Jun. 7, 1995 (ELL-014B).

Originally filed specification for U.S. Appl. No. 08/033,468, filed Mar. 18, 1993 (ELL-006/Con).

Originally filed specification for U.S. Appl. No. 08/462,531, filed Jun. 5, 1995 (ELL-012AA).

Originally filed specification for U.S. Appl. No. 08/473,212, filed Jun. 7, 1995 (ELL-012B).

Description of adidas badminton shoe pre-1989(?), 1 page.

The Reebok Lineup, Fall 1987, 2 pages.

Cavanagh et al., "Biological Aspects of Modeling Shoe/Foot Interaction During Running," *Sport Shoes and Playing Surfaces: Biomechanical Proper ties*, Champaign, IL, © 1984, pp. 24-25, 32-35, and 46-47.

Blechschmidt, "The Structure of the Calcaneal Padding," *Foot & Ankle*, © 1982, Official Journal of the American Orthopaedic Foot Society, Inc., pp. 260-283.

Cavanagh, *The Running Shoe Book*, Mountain View, CA, © 1980, pp. 176-180.

Williams, "Walking on Air," *Case Alumnus*, Fall 1989, vol. LXVII, No. 6, pp. 4-8.

Brooks advertisement, *Runner's World*, Jun. 1989, p. 56+3pp.

Nigg et al., "Influence of Heel Flare and Midsole Contruction on Pronation, Supination, and Impact Forces for Heel-Toe Running," *International Journal of Sport Biomechancis*, 1988, vol. 4, No. 3, pp. 205-219.

Nigg et al., "The influence of lateral heel flare of running shoes on pronation and impact forces," *Medicine and Science in Sports and Exercise*, © 1987, vol. 19, No. 3, pp. 294-302.

Ellis, III, *Executive Summary*, two pages with Figures I-VII attached.

* cited by examiner

(57)   **ABSTRACT**

In its simplest conceptual form, the applicant's invention is the structure of a conventional shoe sole that has been modified by having its sides bent up so that their inner surface conforms to a shape nearly identical but slightly smaller than the shape of the outer surface of the sides of the foot sole of the wearer (instead of the shoe sole sides conforming to the ground by paralleling it, as is conventional). The shoe sole sides are sufficiently flexible to bend out easily when the shoes are put on the wearer's feet and therefore the shoe soles gently hold the sides of the wearer's foot sole when on, providing the equivalent of custom fit in a mass-produced shoe sole. This invention can be applied to shoe sole structures based on a theoretically ideal stability plane as a basic concept, especially including structures exceeding that plane. The theoretically ideal stability plane is defined as the plane of the surface of the bottom of the shoe sole, wherein the shoe sole conforms to the natural shape of the wearer's foot sole, particularly its sides, and has a constant thickness in frontal or transverse plane cross sections.

21 Claims, 30 Drawing Sheets
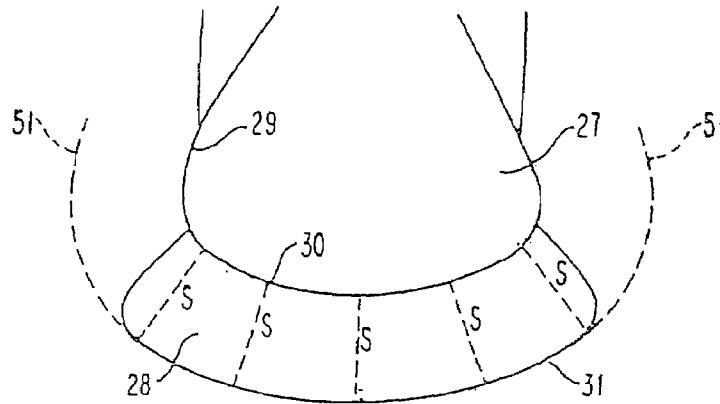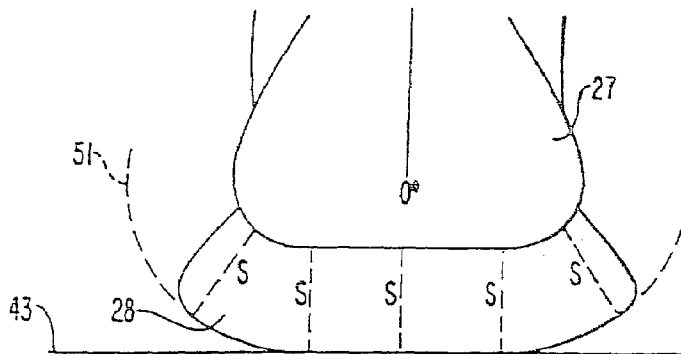
FIG. 1A
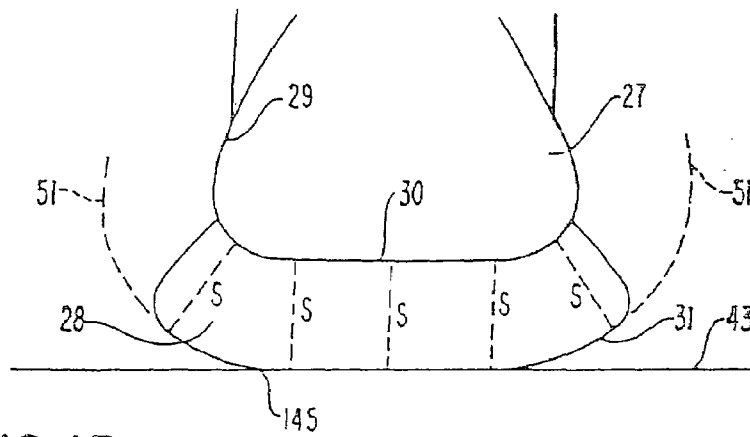
FIG. 1B
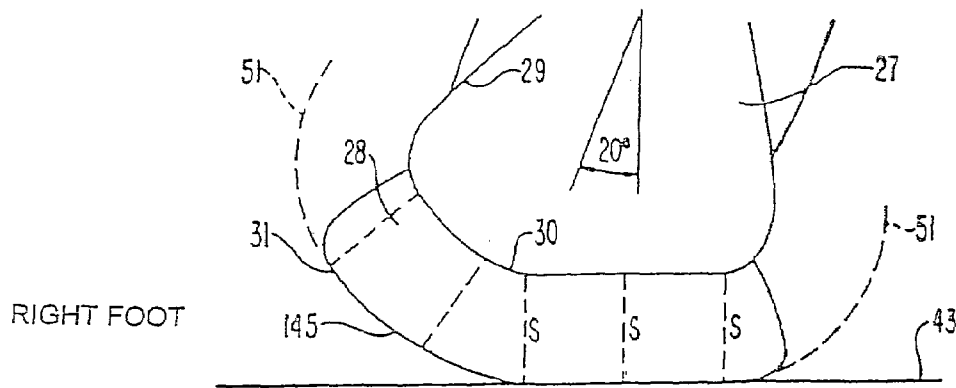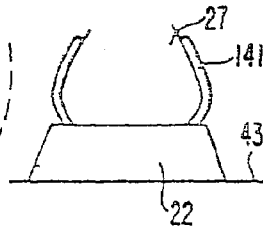

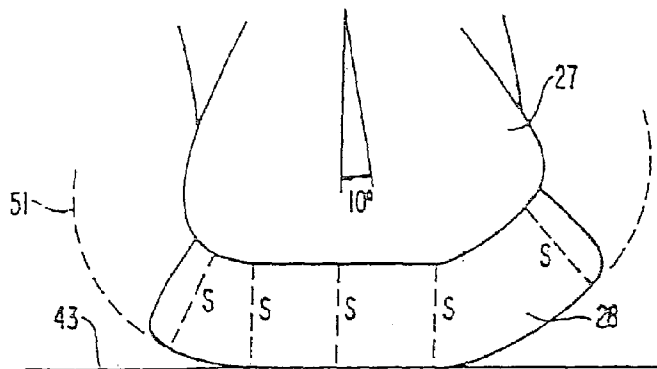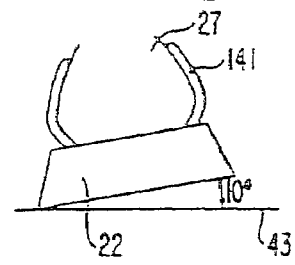
RIGHT FOOT

FIG. 1C

FIG.1D
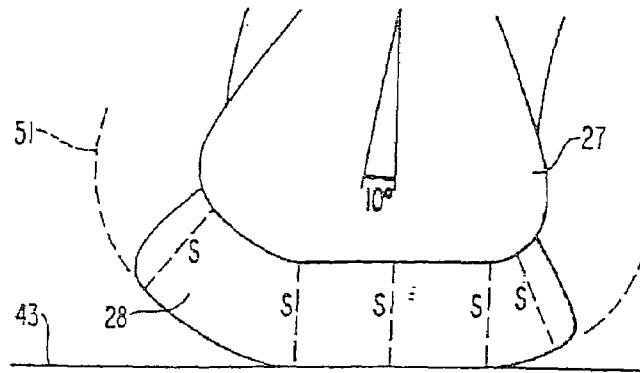
FIG.1G
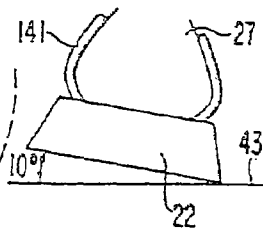
FIG.1E

FIG.1H

FIG.1F

FIG.1I

RIGHT FOOT

(Hatching density
corresponds to
shoe sole density
i.e. relative firmness)

27

29

51   28   28   51

30

31   43

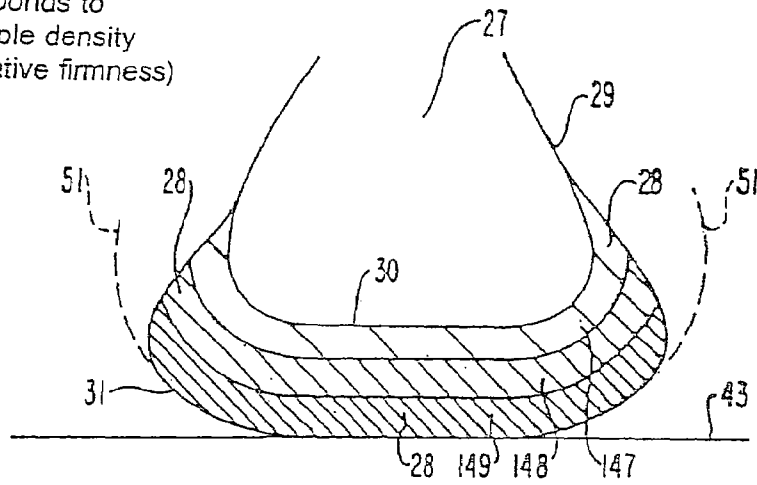28 149 148   147

FIG. 2

29   29

21   21

32   32   51

30   30   30

29   29

51   31

51   28   43

31

31

FIG. 3

FIG. 4

FIG. 5

(Midsoles only
shown)

Frontal Plane
Cross Section
at Heel
(Ankle Joint)

(d¹ is firmer
than d;
d² firmest.

Scale:
Life Size
(Typical
Amer. Size
Men's 10D)

FIG. 6

FIG. 7

FIG. 8

UNLOADED,
UPRIGHT

LOW
PRESSURE

FIG. 9

29

21

32

30

30

30

51

sagittal
variation

51

29

29

28

lesser
also

31

31

43

31

FIG. 10

29

21

21

29

32

d

51

d¹

30

30

30

32

51

51

d²

28

d¹

31

31

43

d¹

31

d

d²
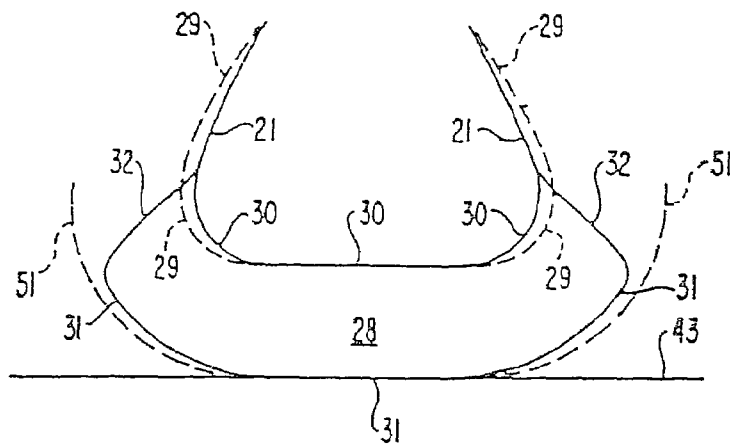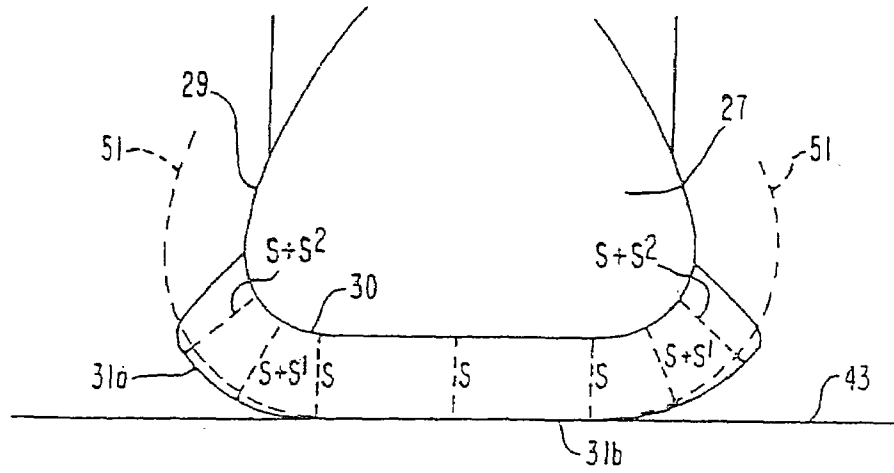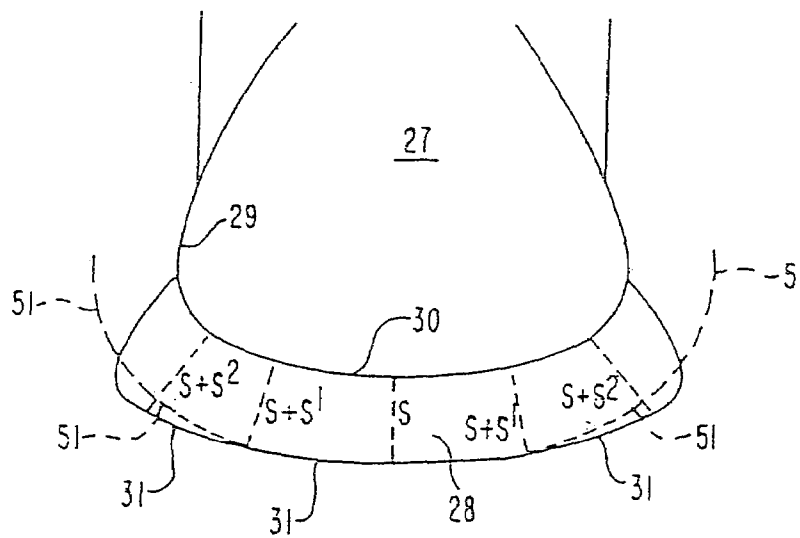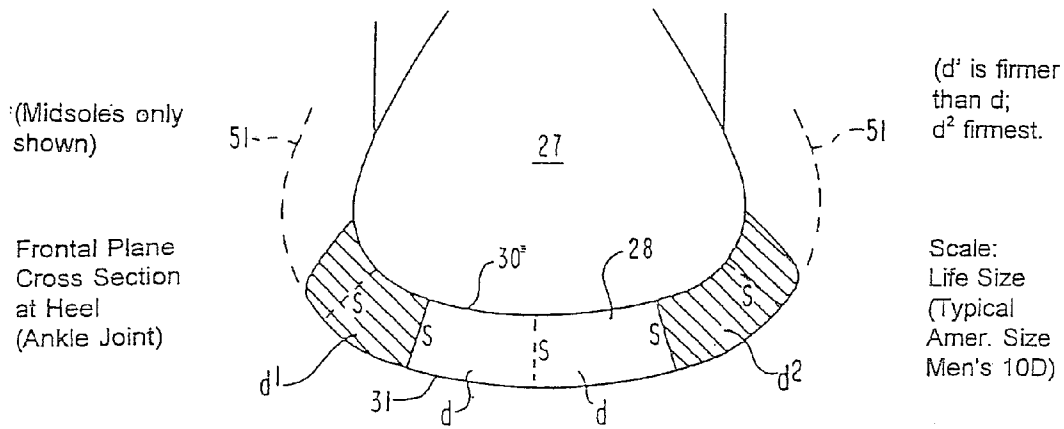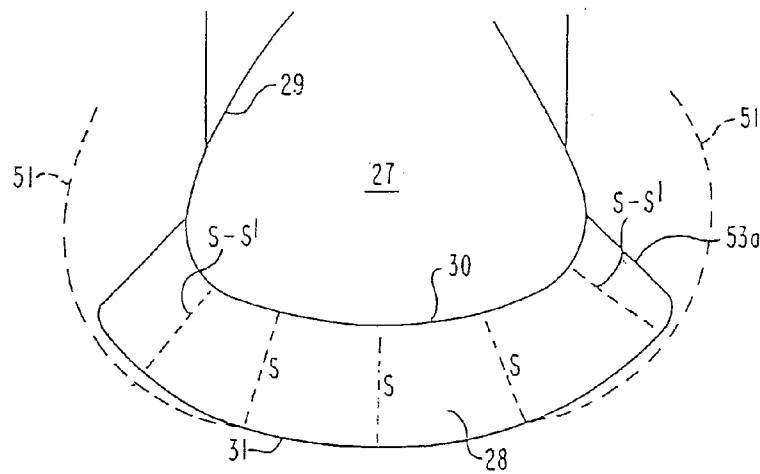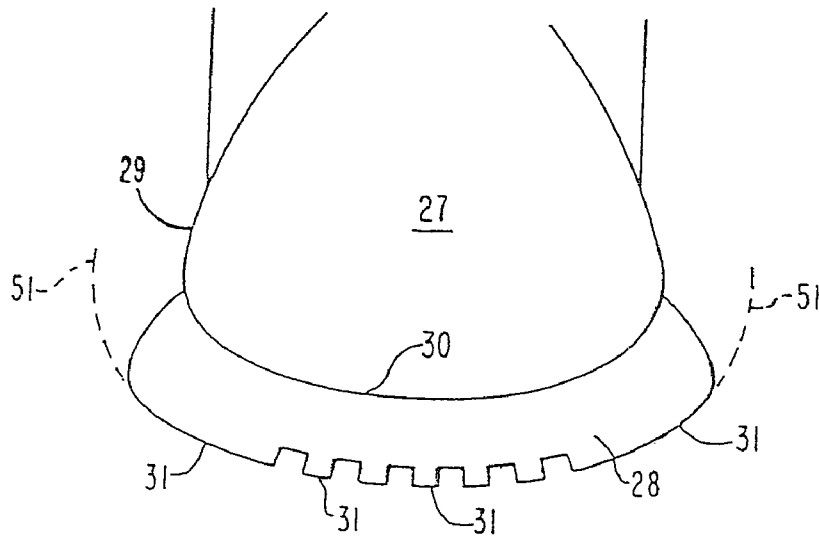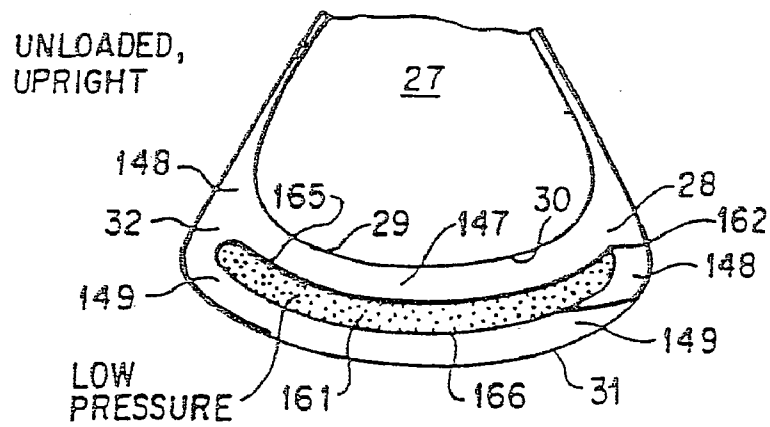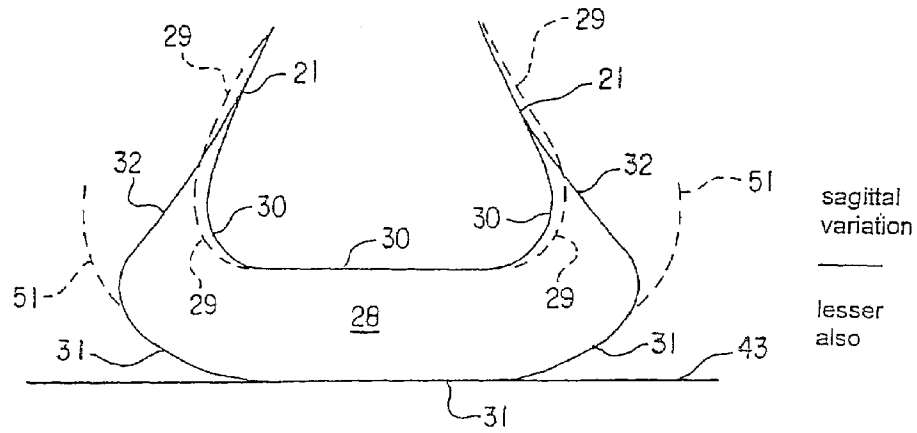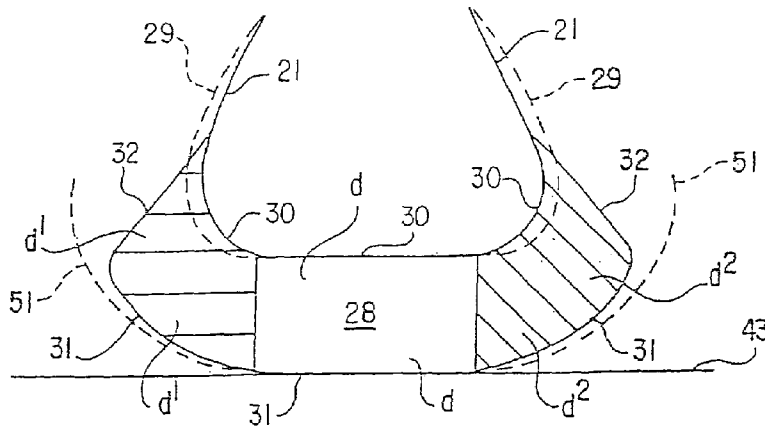
FIG. 11

midsole only
Fig. 2
densitie
suppimpo.
also
hatching is d

FIG. 12

FIG. 13

FIG. 14A

UNSUPPORTED

45°

FIG. 14B
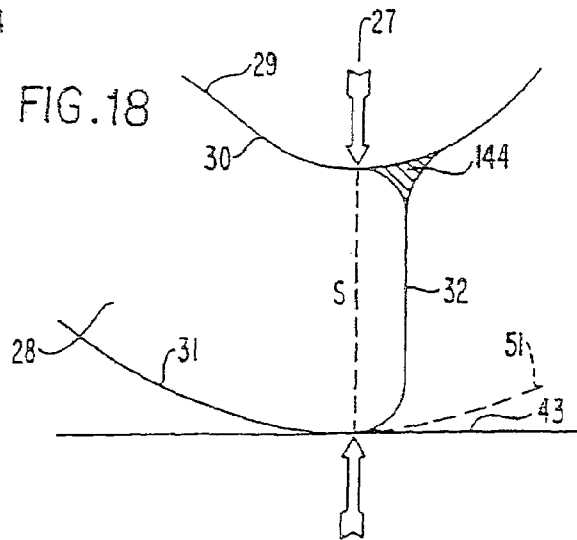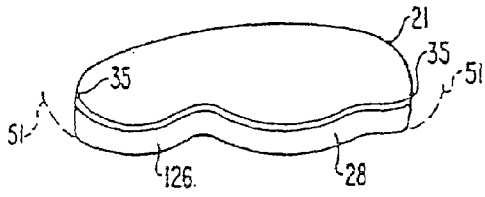

133=1.0

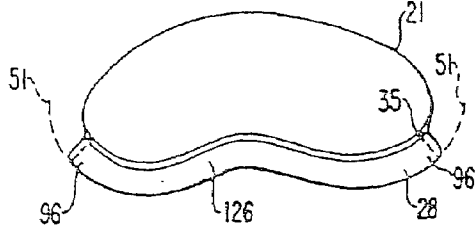135=.7 136=.7

137 138
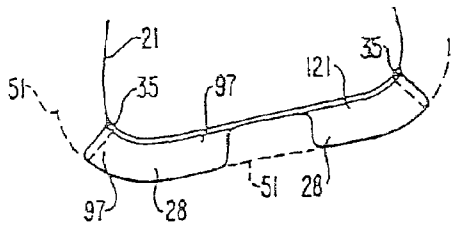=.5 =.5
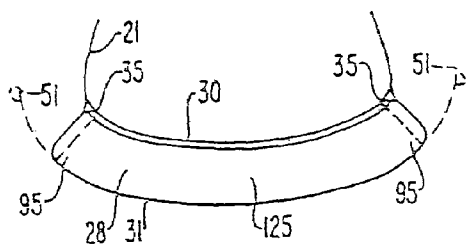
FIG. 15

0° 45°

90°
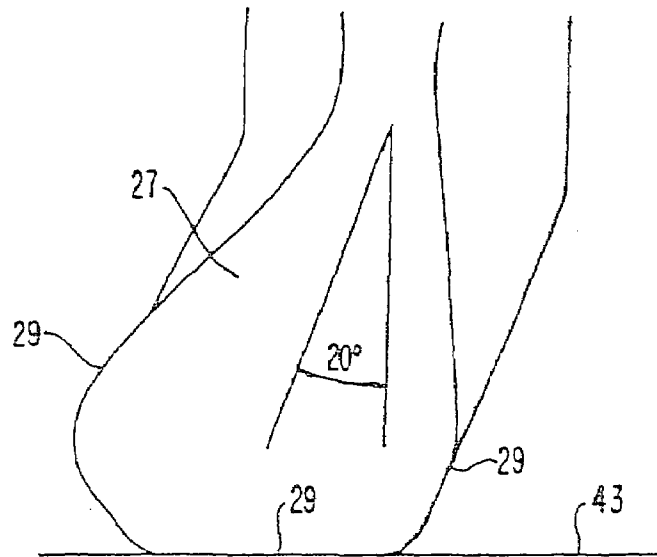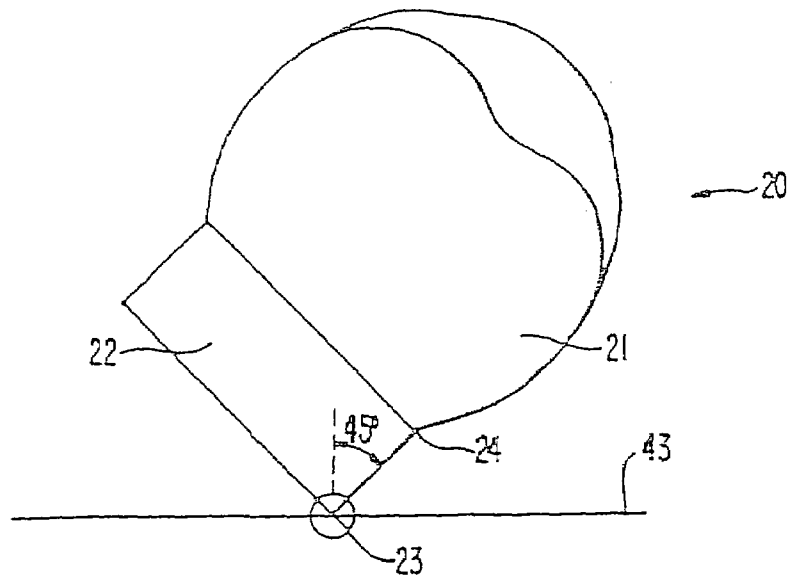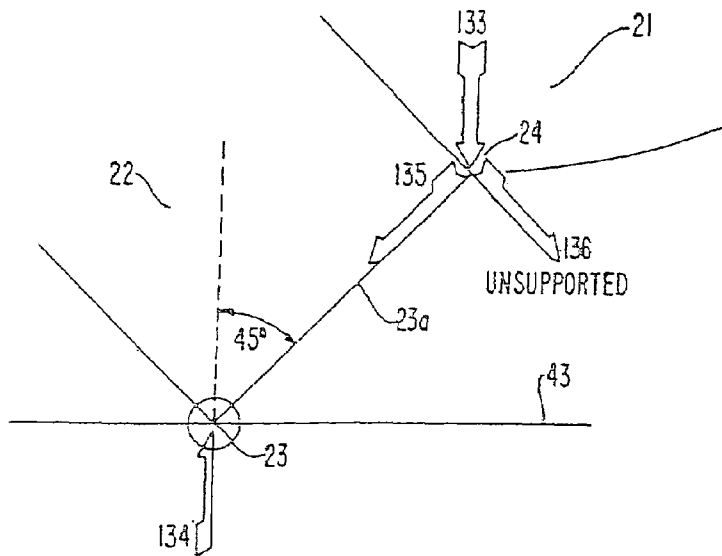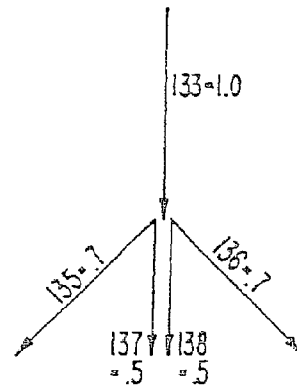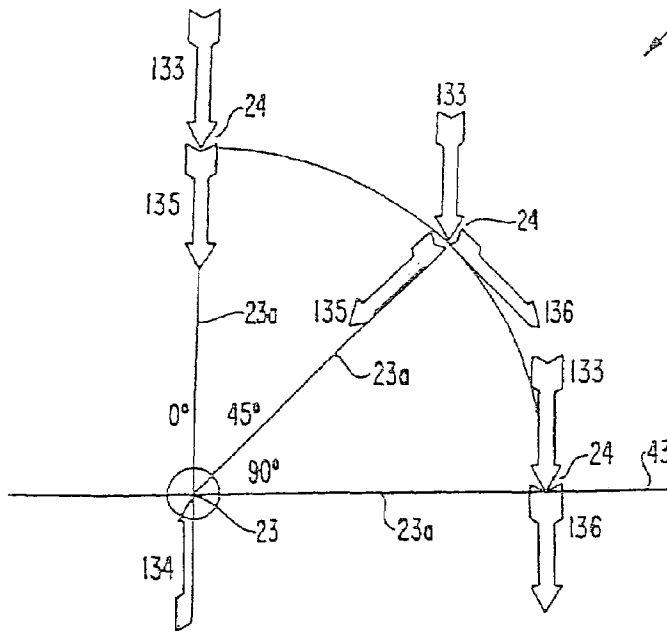
FIG.16
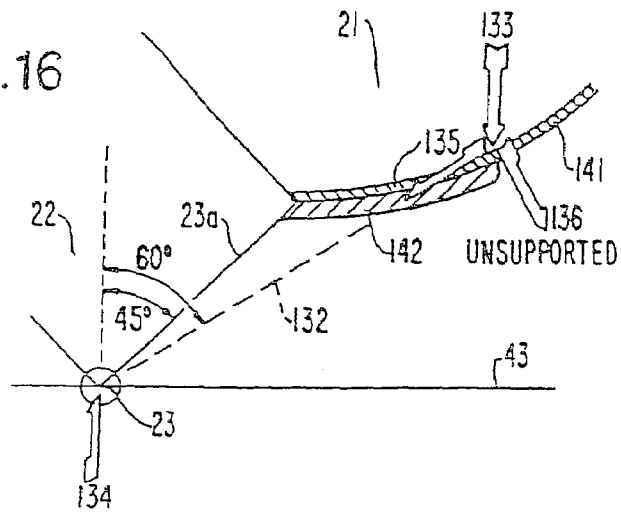
FIG.17
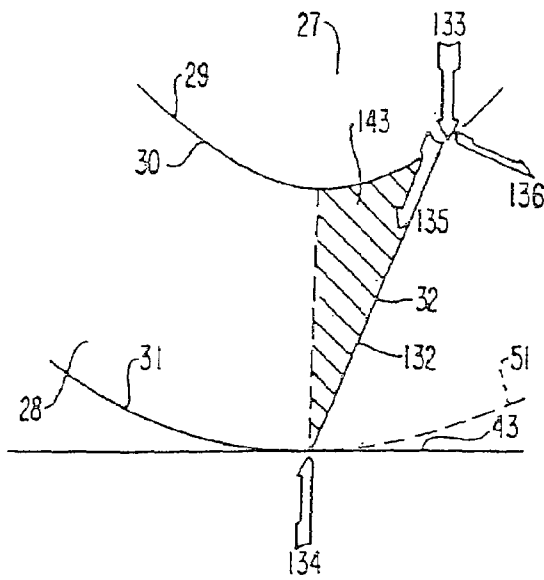
FIG.18

FIG. 19A

FIG. 19B

FIG. 19C

FIG. 19D

FIG. 19E

FIG. 19*E'*

FIG. 19*J*

FIG. 19*F*

FIG. 19*G*

FIG. 19*H*

FIG. 19*I*
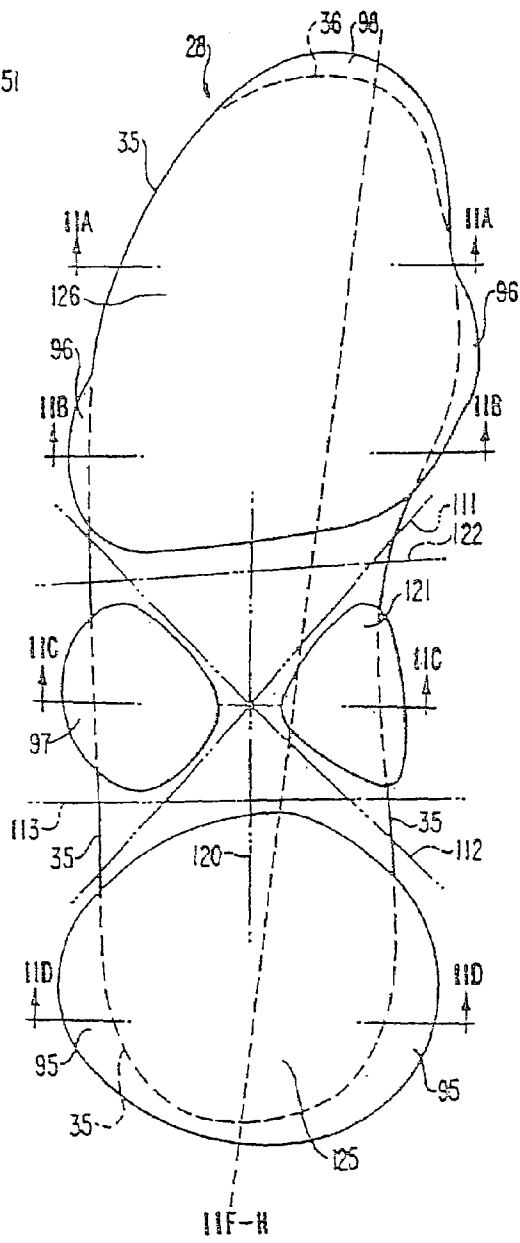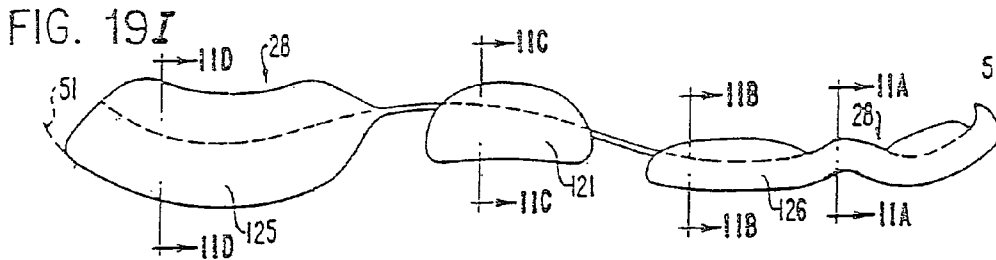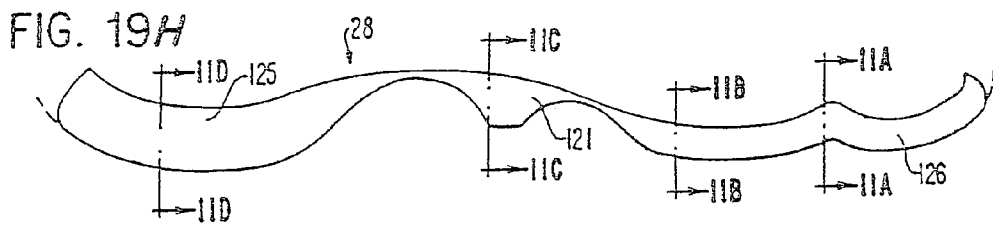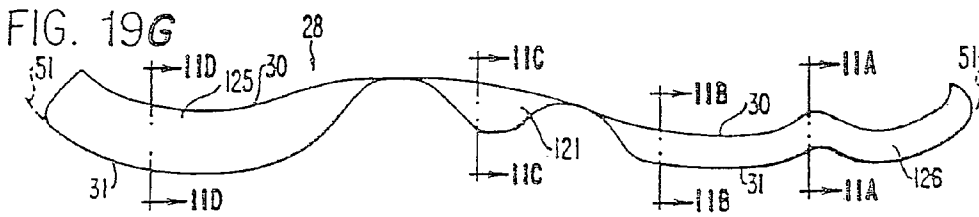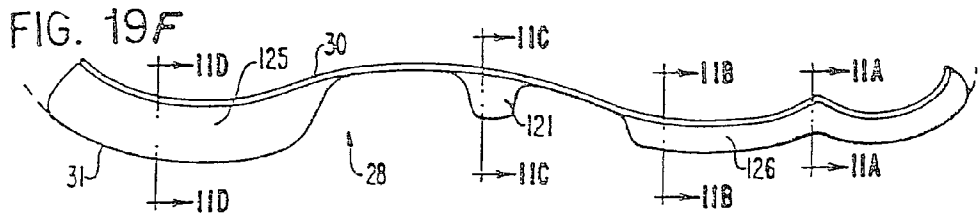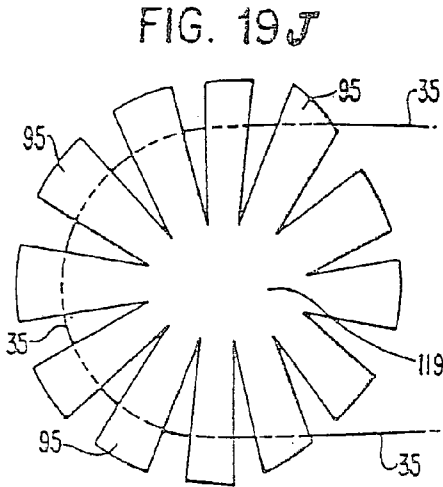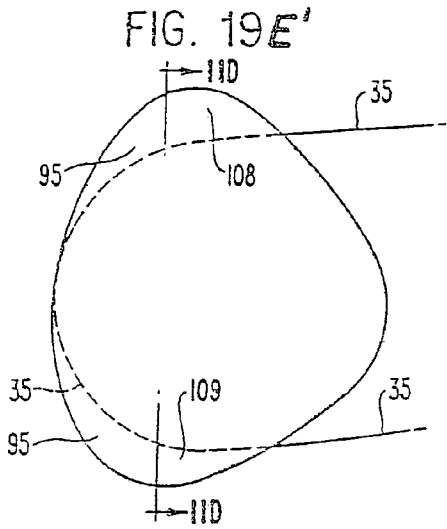
FIG.20
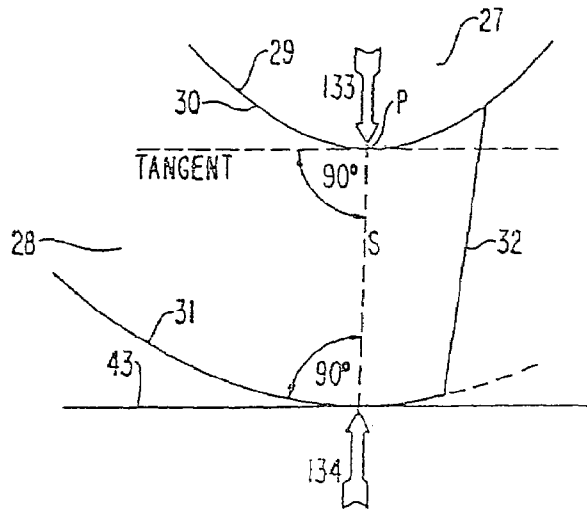
FIG. 21A

FIG. 21C

FIG. 21D
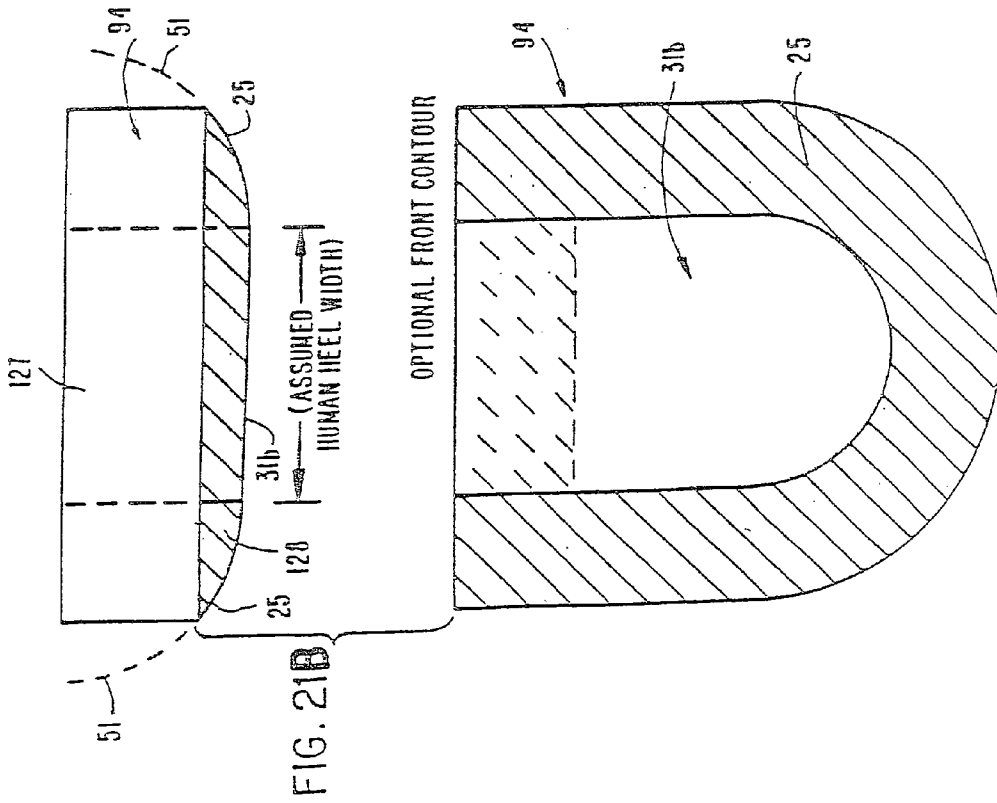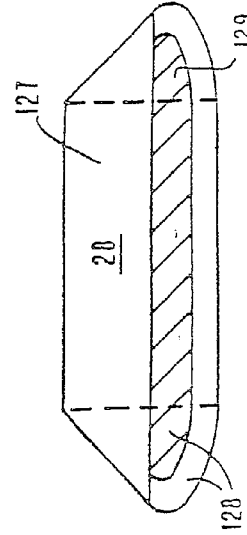
FIG. 21B
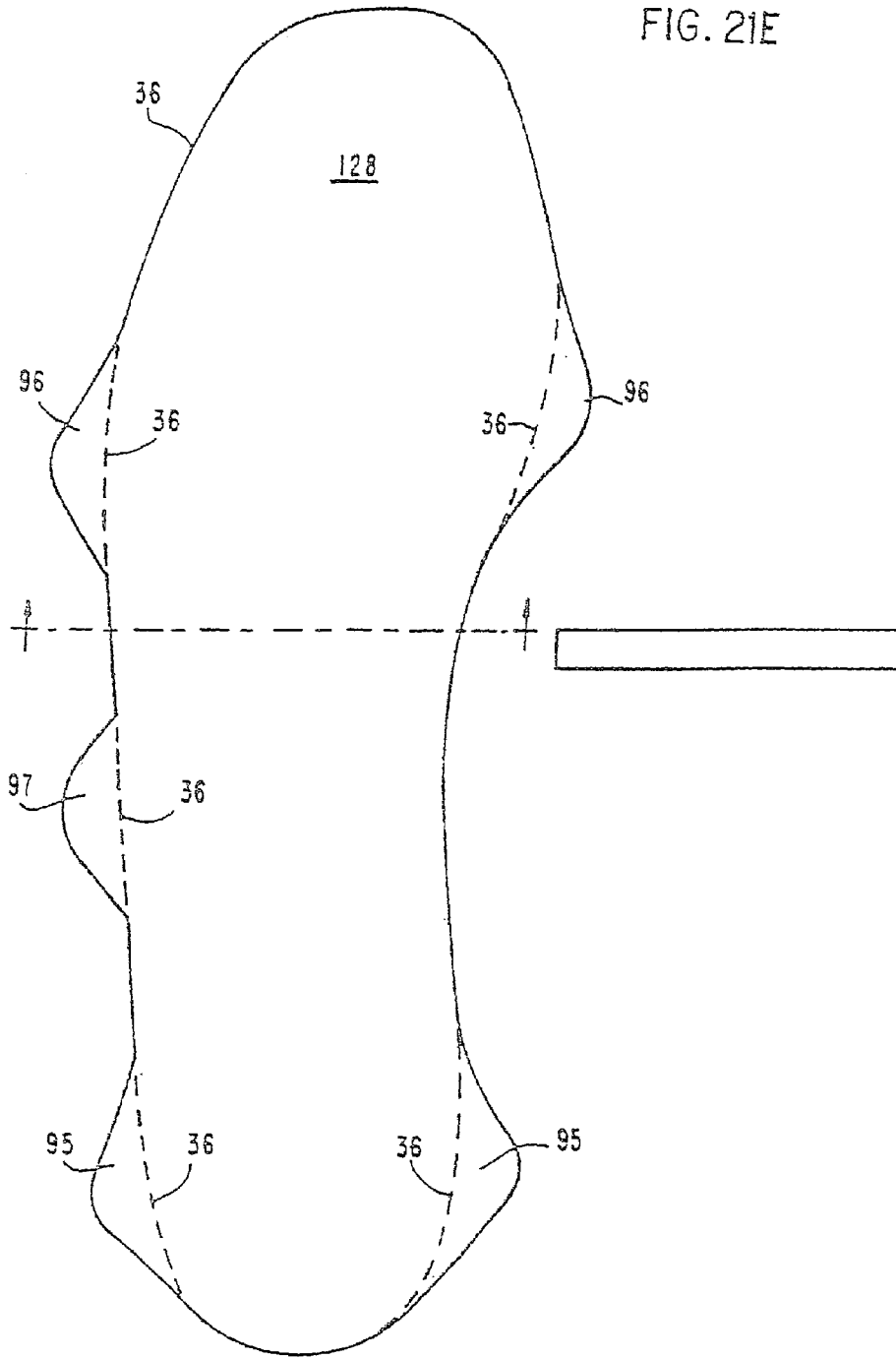
(ASSUMED HUMAN HEEL WIDTH)

OPTIONAL FRONT CONTOUR

FIG. 21E

FIG. 22A

21 — 29   27   29 — 21

22

FIG. 22B

21

131   41   41   131

r   r

51   51

s s   s s

51   51

22

FIG. 22C

21

131   131

s s   s s

26   26

28b

FIG. 23A

21

27

29   29

22

FIG. 23B

21

131   131

s   s

s   s   s   s

51   51

22

FIG. 23C

21

131   131

s   s   s   s

28a   28   28a

FIG. 24

FIG. 25

FIG. 26A

54   52   53

26

54a

50,51   50,51

FIG. 26B

54

53a

51

56

50a   54a   50a

FIG. 26C

53a

23a

51

56

50b   54a   50b
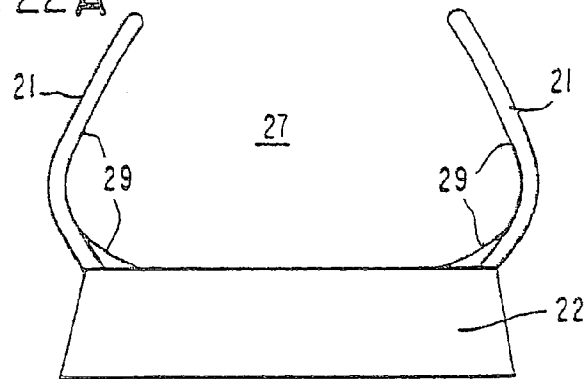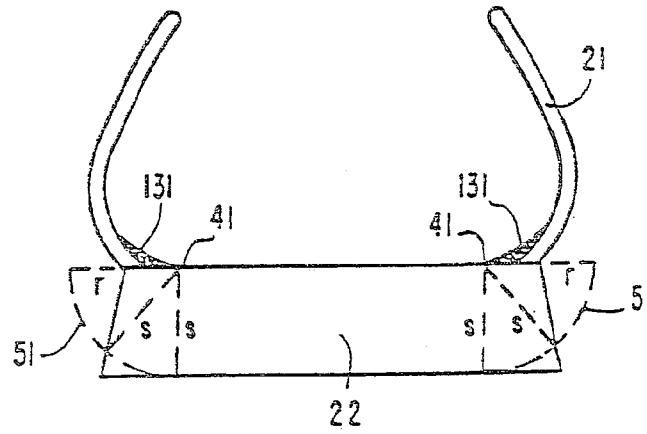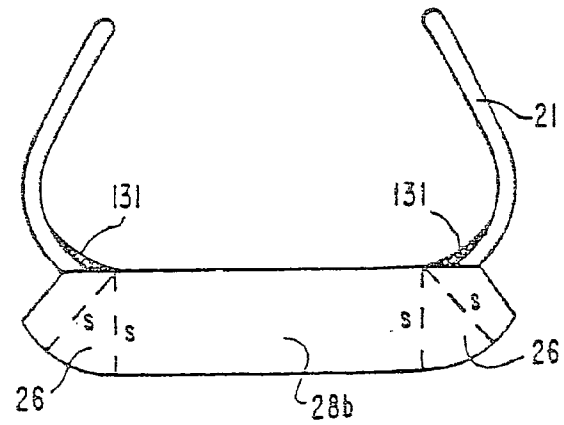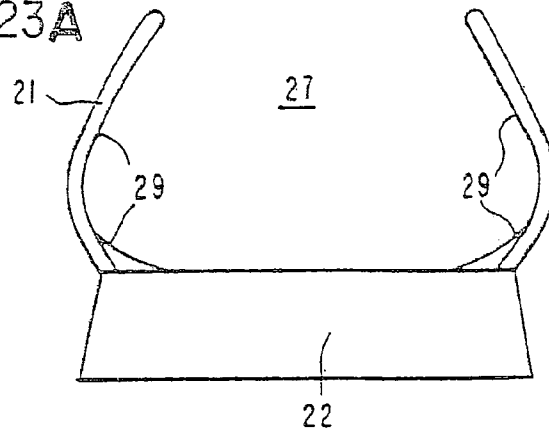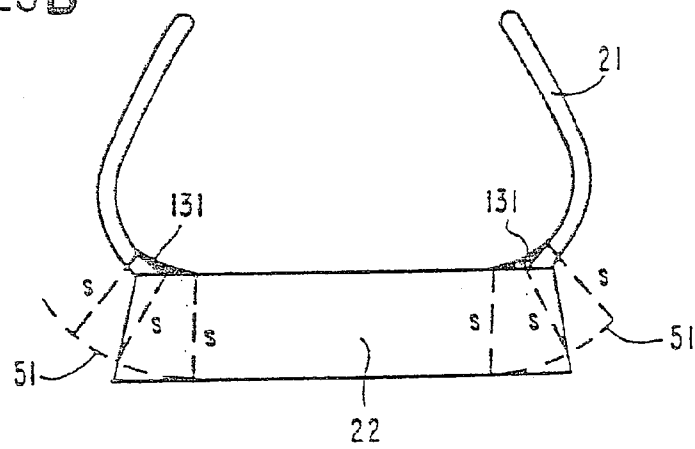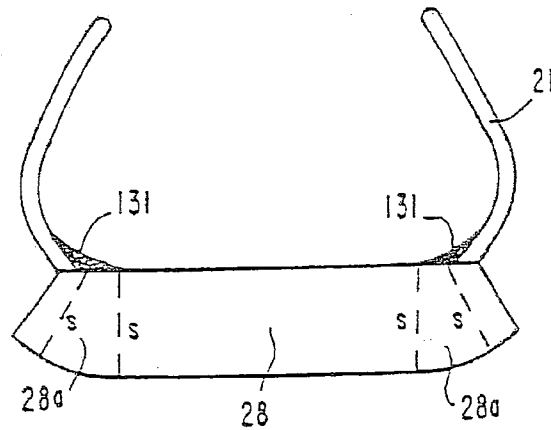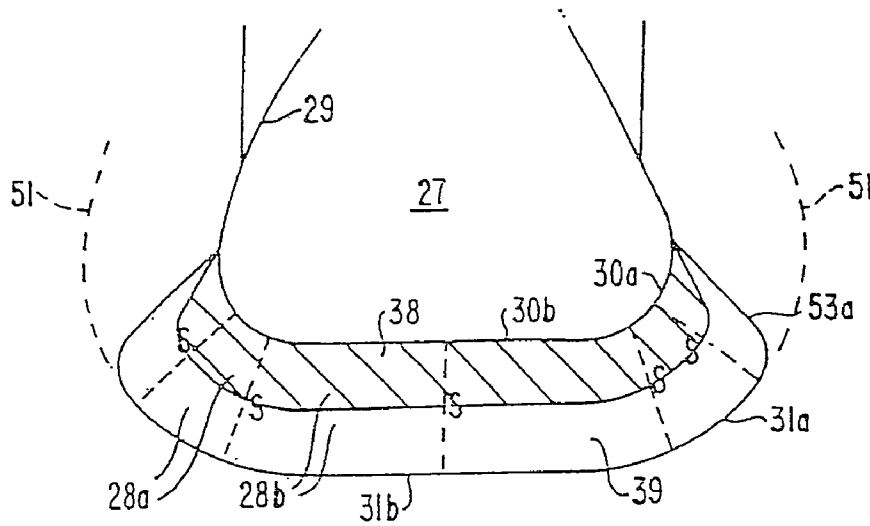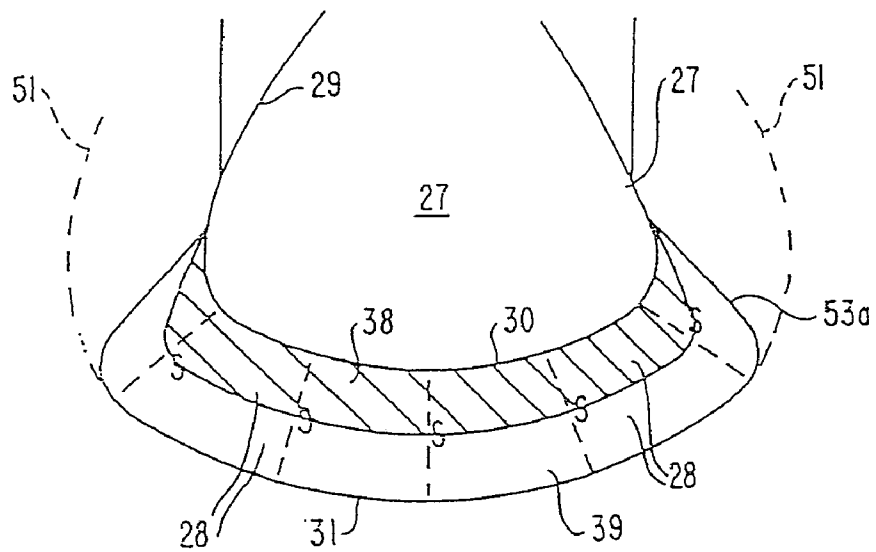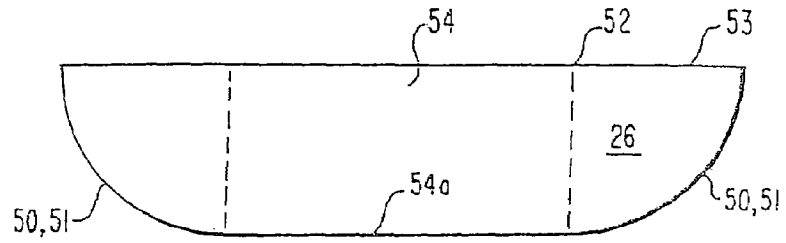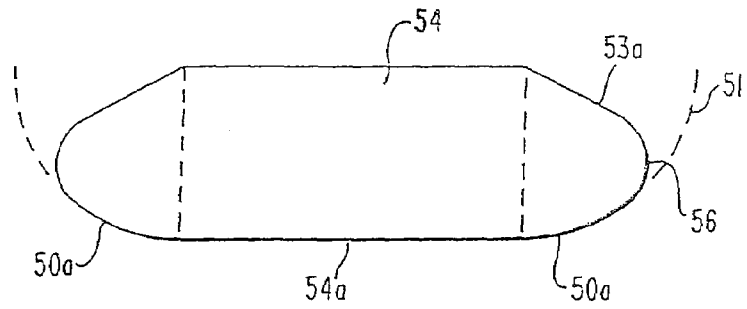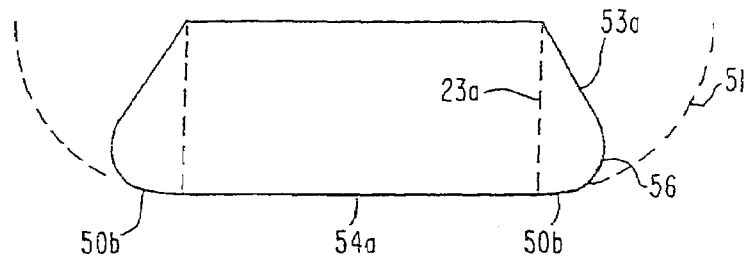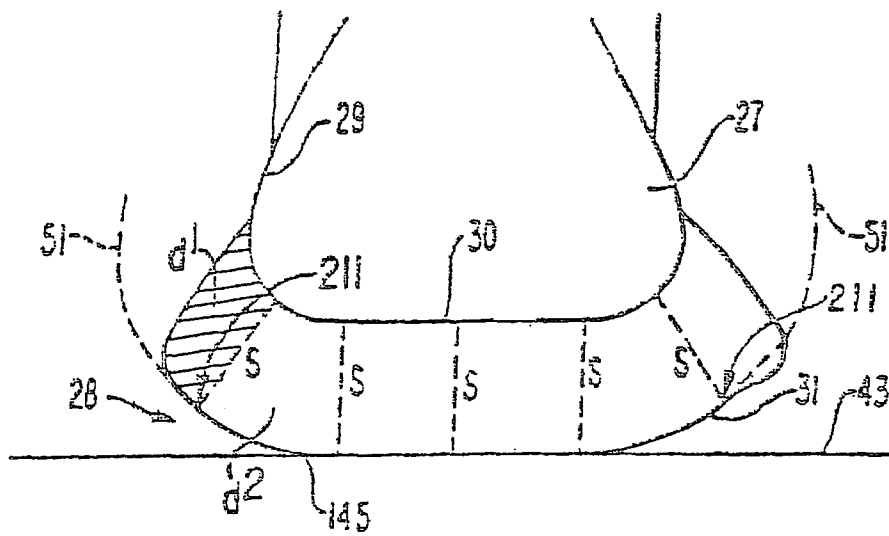
FIG. 27

FIG. 28

FIG. 29

FIG. 30

FIG. 31

29   27

C^l 41   30b   41 C^l
$S^l + S$ $\odot$ $S + S^l$
51   C   I   C   51
S   IS   S^l
25^l 25^l
31b   27   26

FIG. 32

27

r30b
51   51
s   d   IS   d   S
d^l 25   31b   27   25 d^l

FIG. 33A

29

51

27

30a   S-S¹

51

S-S¹   30b   53a

S   28   S   S¹   31a

31b   28b   28a

FIG. 33B

29

51

51   27

S-S¹   S-S¹

30   53a

S   S   S

31   28

FIG. 33C

27

C   C¹   C¹   C

S-S¹   30b   S-S¹

51   51

S   S   S¹   25¹

51   26

31b   27
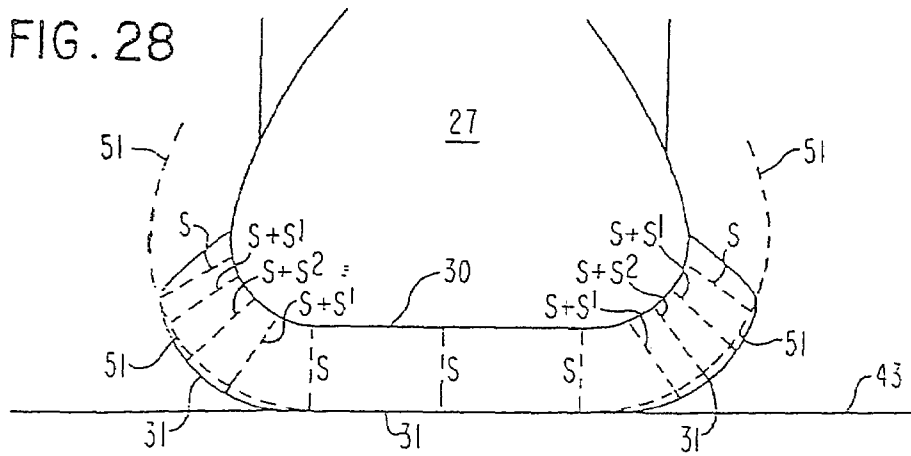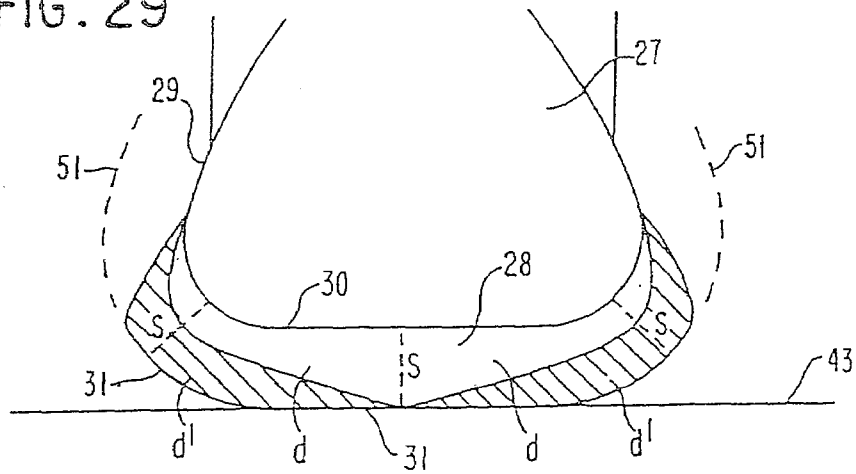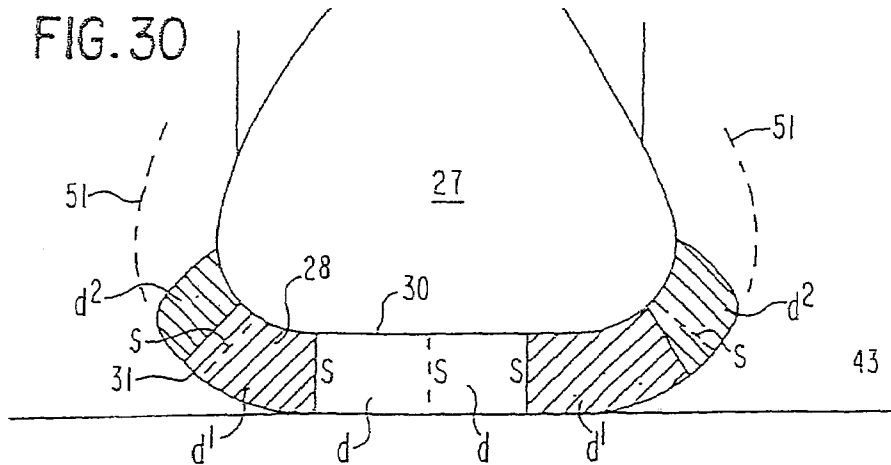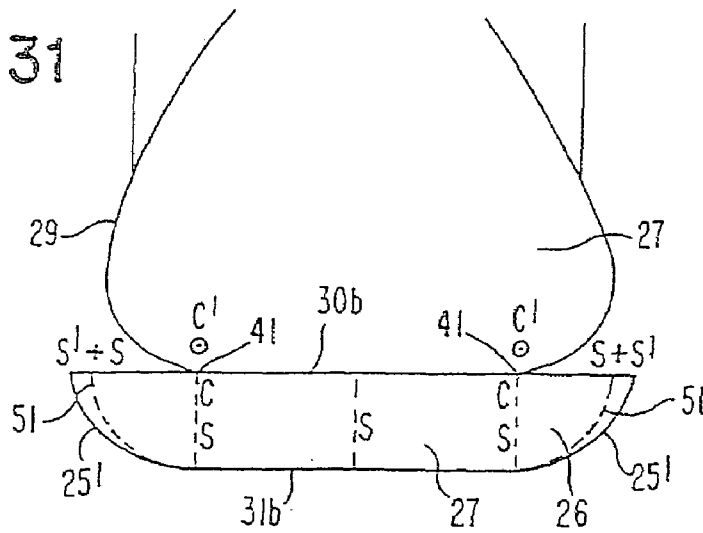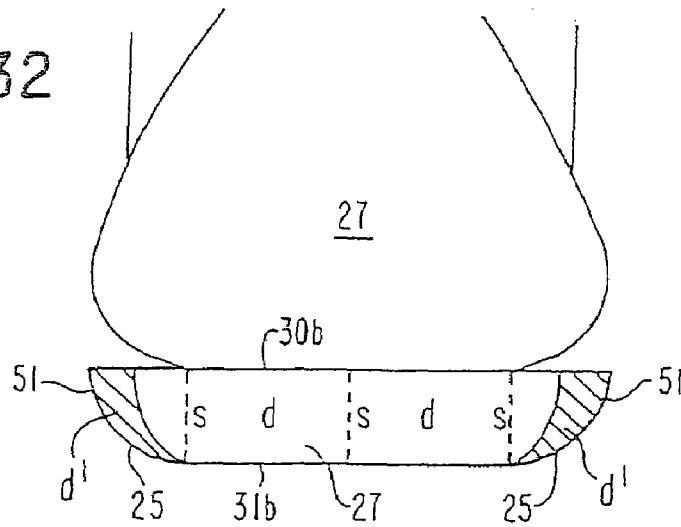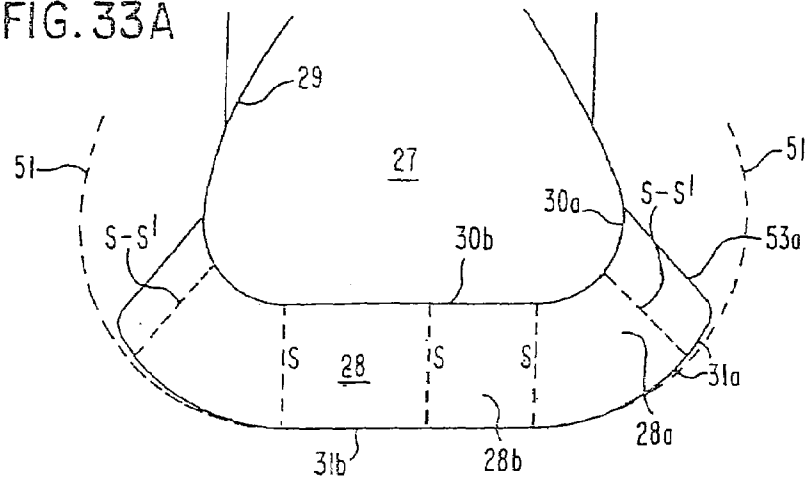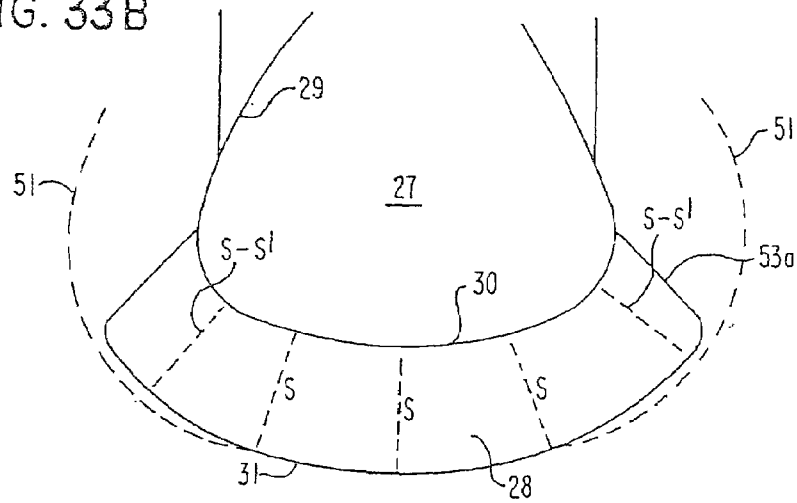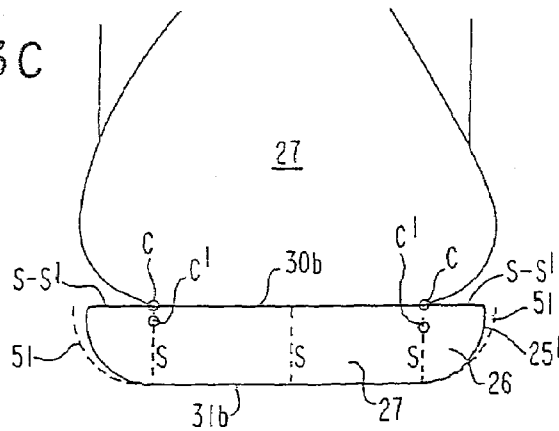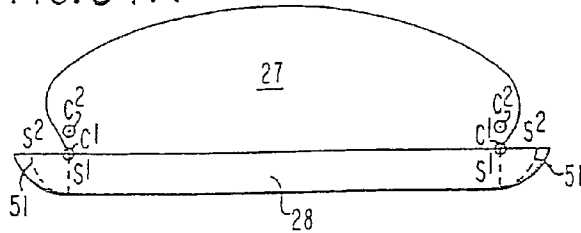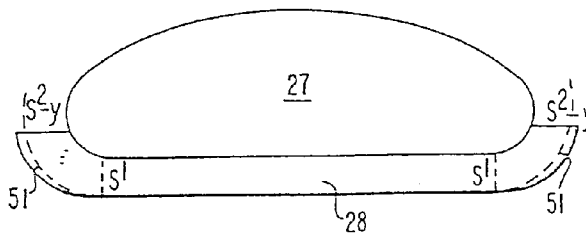
FIG. 34A
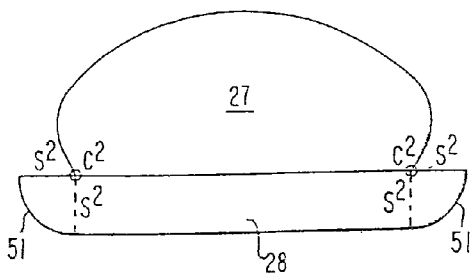
FIG. 34B
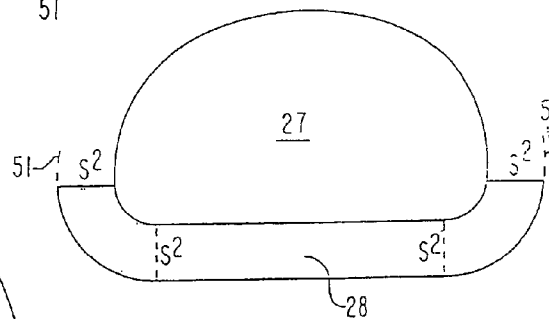
FIG. 34C
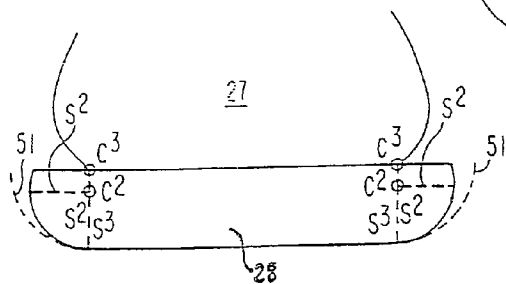
FIG. 34D

FIG. 34E

FIG. 34F

FIG. 35

(PRIOR ART)

FIG. 36

TENSION

LEVER ARM

PIVOTING EDGE

FIG. 37

TENSION

LEVER ARM

FIG. 38

27

20°

29

29

150

TENSION

COMPRESSION

43

FIG. 39A

29

27

21

21

32

31

21   30   28   21

43

149

FIG. 39B

21

32

149

43

FIG. 40

155b

27

29

150

30

21

28

32   147

148

155a

31   43

149

FIG. 41

32

27

29

31

30   TENSION

128   28   32

43

COMPRESSION

FIG. 42A
UNLOADED,
UPRIGHT

159
167
27
163
29
158
160
160
LOW PRESSURE   29   168

FIG. 42B
LOADED
MODERATELY,
UPRIGHT

158
159
167
27
163
29
TENSION
43
TENSION
COMPRESSION   168
PRESSURE (MEDIUM)

FIG. 42C
LOADED
HEAVILY,
UPRIGHT

159
163   163
27
158
TENSION
TENSION
43
29
COMPRESSION   160   29
PRESSURE
(HIGH)

FIG. 42D
LOADED
HEAVILY,
20° LATERAL
TILT

167
158
20°
159
29
27
163
TENSION
43
TENSION   29 168   COMPRESSION
PRESSURE (HIGH)

UNLOADED,
UPRIGHT

FIG. 43A

LOADED
MODERATED,
UPRIGHT

FIG. 43B

LOADED
HEAVILY,
UPRIGHT

FIG. 43C

LOADED HEAVILY,
20° LATERAL TILT

FIG. 43D

FIG. 44A

FIG. 44B

FIG. 44C

SHOES SOLE STRUCTURES

This application is a divisional of U.S. patent application Ser. No. 09/974,786 filed Oct. 12, 2001, now U.S. Pat. No. 6,729,046, which is a divisional of U.S. patent application Ser. No. 09/907,598 filed Jul. 19, 2001, now U.S. Pat. No. 6,591,519; which is a divisional of U.S. patent application Ser. No. 09/734,905 filed Dec. 13, 2000, now U.S. Pat. No. 6,308,439; which is a continuation of U.S. patent application Ser. No. 08/477,954 filed Jun. 7, 1995, now U.S. Pat. No. 6,163,982; which is a continuation-in-part of U.S. patent application Ser. No. 08/376,661 filed Jan. 23, 1995, now U.S. Pat. No. 6,810,606; which is a continuation of U.S. patent application Ser. No. 08/127,487 filed Sep. 28, 1993, now abandoned; which is a continuation of U.S. patent application Ser. No. 07/729,886 filed Jul. 11, 1991, now abandoned; which is a continuation of U.S. patent application Ser. No. 07/400,714 filed Aug. 30, 1989, now abandoned.

BACKGROUND OF THE INVENTION

This invention relates generally to the structure of soles of shoes and other footwear, including soles of street shoes, hiking boots, sandals, slippers, and moccasins. More specifically, this invention relates to the structure of athletic shoe soles, including such examples as basketball and running shoes.

More particularly, in it simplest conceptual form, this invention is the structure of a conventional shoe sole that has been modified by having its sides bent up so that their inner surface conforms to a shape nearly identical but slightly smaller than the shape of the outer surface of the sides of the foot sole of the wearer (instead of the shoe sole sides conforming to the ground by paralleling it, as is conventional). The shoe sole sides are sufficiently flexible to bend out easily when the shoes are put on the wearer's feet and therefore the shoe soles gently hold the sides of the wearer's foot sole when on, providing the equivalent of custom fit in a mass-produced shoe sole.

Still more particularly, this invention relates to variations in the structure of such soles using a theoretically ideal stability plane as a basic concept, especially including structures exceeding that plane.

The parent '598 application clarified and expanded the applicant's earlier filed U.S. application Ser. No. 07/680,134, filed Apr. 3, 1991.

The applicant has introduced into the art the concept of a theoretically ideal stability plane as a structural basis for shoe sole designs. The theoretically ideal stability plane was defined by the applicant in previous copending applications as the plane of the surface of the bottom of the shoe sole, wherein the shoe sole conforms to the natural shape of the wearer's foot sole, particularly its sides, and has a constant thickness in frontal or transverse plane cross sections. Therefore, by definition, the theoretically ideal stability plane is the surface plane of the bottom of the shoe sole that parallels the surface of the wearer's foot sole in transverse or frontal plane cross sections.

The theoretically ideal stability plane concept as implemented into shoes such as street shoes and athletic shoes is presented in U.S. Pat. No. 4,989,349, issued Feb. 5, 1991 and U.S. Pat. No. 5,317,819, issued Jun. 7, 1994, both of which are incorporated by reference; and pending U.S. application Ser. No. 07/400,714, filed Aug. 30, 1989; U.S. Ser. No. 07/416,478, filed Oct. 3, 1989; U.S. Ser. No. 07/424,509, filed Oct. 20, 1989; U.S. Ser. No. 07/463,302,

filed Jan. 10, 1990; U.S. Ser. No. 07/469,313, filed Jan. 24, 1990; U.S. Ser. No. 07/478,579, filed Feb. 8, 1990; U.S. Ser. No. 07/539,870, filed Jun. 18, 1990; and U.S. Ser. No. 07/608,748, filed Nov. 5, 1990.

PCT applications based on the above patents and applications have been published as WO 90/00358 of Jan. 25, 1990 (part of the '349 Patent, all of the '819 Patent and part of '714 application); WO 91/03180 of Mar. 21, 1991 (the remainder of the '714 application); WO 91/04683 of Apr. 18, 1991 (the '478 application); WO 91/05491 of May 02, 1991 (the '509 application); WO 91/10377 of Jul. 25, 1991 (the '302 application); WO 91/11124 of Aug. 08, 1991 (the '313 application); WO 91/11924 of Aug. 22, 1991 (the '579 application); WO 91/19429 of Dec. 26, 1991 (the '870 application); WO 92/07483 of May 14, 1992 (the '748 application); WO 92/18024 of Oct. 29, 1992 (the '598 application); and WO 94/03080 of Feb. 17, 1994 (the '523 application). All of above publications are incorporated by reference in this application to support claimed prior inventions that are incorporated in combinations with other elements disclosed in the incorporated applications.

This new invention is a modification of the inventions disclosed and claimed in the earlier applications and develops the application of the concept of the theoretically ideal stability plane to other shoe structures. Each of the applicant's applications is built directly on its predecessors and therefore all possible combinations of inventions or their component elements with other inventions or elements in prior and subsequent applications have always been specifically intended by the applicant. Generally, however, the applicant's applications are generic at such a fundamental level that it is not possible as a practical matter to describe every embodiment combination that offers substantial improvement over the existing art, as the length of this description of only some combinations will testify.

Accordingly, it is a general object of this invention to elaborate upon the application of the principle of the theoretically ideal stability plane to other shoe structures.

The purpose of this application is to specifically describe some of the most important combinations, especially those that constitute optimal ones, that exist between the applicant's U.S. patent application Ser. No. 07/400,714, filed Aug. 30, 1989, and subsequent patents filed by the applicant, particularly U.S. Ser. No. 07/416,478, filed Oct. 3, 1989, as well as to provide an explicit basis for describing elements from those two applications in combination with any other useful combinations possible from elements disclosed in any of the other incorporated patents, applications, or PCT publications listed above.

The '714 application indicated that existing running shoes are unnecessarily unsafe. They profoundly disrupt natural human biomechanics. The resulting unnatural foot and ankle motion leads to what are abnormally high levels of running injuries.
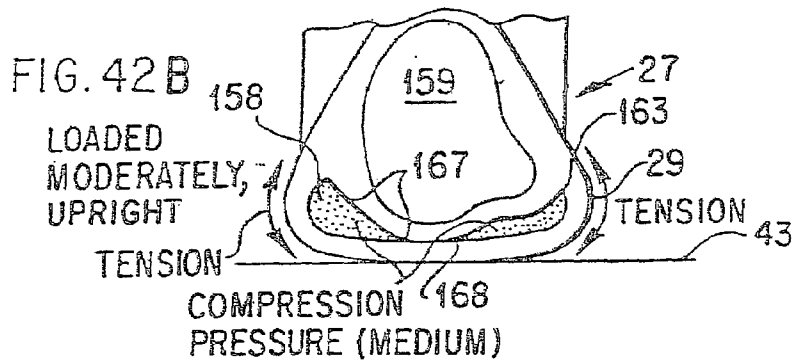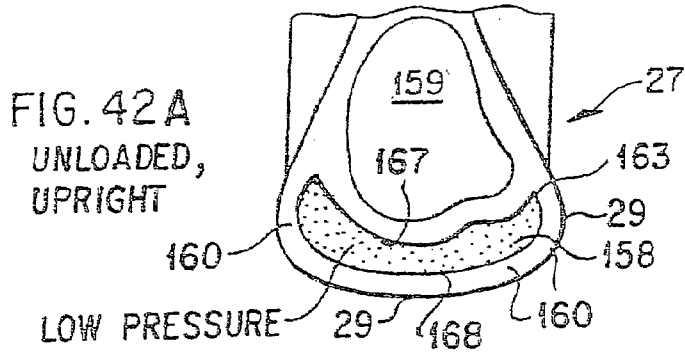
Proof of the unnatural effect of shoes has come quite unexpectedly from the discovery that, at the extreme end of its normal range of motion, the unshod bare foot is naturally stable, almost unsprainable, while the foot equipped with any shoe, athletic or otherwise, is artificially unstable and abnormally prone to ankle sprains. Consequently, ordinary ankle sprains must be viewed as largely an unnatural phenomena, even though fairly common. Compelling evidence demonstrates that the stability of bare feet is entirely different from the stability of shoe-equipped feet.

The underlying cause of the universal instability of shoes is a critical but correctable design flaw. That hidden flaw, so deeply ingrained in existing shoe designs, is so extraordi-

narily fundamental that it has remained unnoticed until now. The flaw is revealed by a novel new biomechanical test, one that is unprecedented in its simplicity. It is easy enough to be duplicated and verified by anyone; it only takes a few minutes and requires no scientific equipment or expertise. The simplicity of the test belies its surprisingly convincing results. It demonstrates an obvious difference in stability between a bare foot and a running shoe, a difference so unexpectedly huge that it makes an apparently subjective test clearly objective instead. The test proves beyond doubt that all existing shoes are unsafely unstable.

The broader implications of this uniquely unambiguous discovery are potentially far-reaching. The same fundamental flaw in existing shoes that is glaringly exposed by the new test also appears to be the major cause of chronic overuse injuries, which are unusually common in running, as well as other sport injuries. It causes the chronic injuries in the same way it causes ankle sprains; that is, by seriously disrupting natural foot and ankle biomechanics.

It was a general object of the '714 invention to provide a shoe sole which, when under load and tilting to the side, deforms in a manner which closely parallels that of the foot of its wearer, while retaining nearly the same amount of contact of the shoe sole with the around as in its upright state.

It was still another object of the '714 invention to provide a deformable shoe sole having the upper portion or the sides bent inwardly somewhat so that when worn the sides bend out easily to approximate a custom fit.

It was still another object of the '714 invention to provide a shoe having a naturally contoured sole which is abbreviated along its sides to only essential structural stability and propulsion elements, which are combined and integrated into the same discontinuous shoe sole structural elements underneath the foot, which approximate the principal structural elements of a human foot and their natural articulation between elements.

The '478 invention relates to variations in the structure of such shoes having a sole contour which follows a theoretically ideal stability plane as a basic concept, but which deviates therefrom outwardly, to provide greater than natural stability. Still more particularly, this invention relates to the use of structures approximating, but increasing beyond, a theoretically ideal stability plane to provide greater than natural stability for an individual whose natural foot and ankle biomechanical functioning have been degraded by a lifetime use of flawed existing shoes.

The '478 invention is a modification of the inventions disclosed and claimed in the earlier application and develops the application of the concePt of the theoretically ideal stability plane to other shoe structures. As such, it presents certain structural ideas which deviate outwardly from the theoretically ideal stability plane to compensate for faulty foot biomechanics caused by the major flaw in existing shoe designs identified in the earlier patent applications.

The shoe sole designs in the '478 application are based on a recognition that lifetime use of existing shoes, the unnatural design of which is innately and seriously flawed, has produced actual structural chances in the human foot and ankle. Existing shoes thereby have altered natural human biomechanics in many, if not most, individuals to an extent that must be compensated for in an enhanced and therapeutic design. The continual repetition of serious interference by existing shoes appears to have produced individual biomechanical chances that may be permanent, so simply removing the cause is not enough. Treating the residual effect must also be undertaken.

Accordingly, it was a general object of the '478 invention to elaborate upon the application of the principle of the theoretically ideal stability plane to other shoe structures.

It was still another object of the '478 invention to provide a shoe having a sole contour which deviates outwardly in a constructive way from the theoretically ideal stability plane.

It was another object of the '478 invention to provide a sole contour having a shape naturally contoured to the shape of a human foot, but having a shoe sole thickness which is increases somewhat beyond the thickness specified by the theoretically ideal stability plane.

It is another object of this invention to provide a naturally contoured shoe sole having a thickness somewhat greater than mandated by the concept of a theoretically ideal stability plane, either through most of the contour of the sole, or at preselected portions of the sole.

It is yet another object of this invention to provide a naturally contoured shoe sole having a thickness which approximates a theoretically ideal stability plane, but which varies toward either a greater thickness throughout the sole or at spaced Portions thereof, or toward a similar but lesser thickness.

The '302 invention relates to a shoe having an anthropomorphic sole that copies the underlying support, stability and cushioning structures of the human foot. Natural stability is Provided by attaching a completely flexible but relatively inelastic shoe sole upper directly to the bottom sole, enveloping the sides of the midsole, instead of attaching it to the top surface of the shoe sole. Doing so puts the flexible side of the shoe upper under tension in reaction to destabilizing sideways forces on the shoe causing it to tilt. That tension force is balanced and in equilibrium because the bottom sole is firmly anchored by body weight, so the destabilizing sideways motion is neutralized by the tension in the flexible sides of the shoe upper. Still more particularly, this invention relates to support and cushioning which is provided by shoe sole compartments filled with a pressure-transmitting medium like liquid, gas, or gel. Unlike similar existing systems, direct physical contact occurs between the upper surface and the lower surface of the compartments, providing firm, stable support. Cushioning is provided by the transmitting medium progressively causing tension in the flexible and semi-elastic sides of the shoe sole. The compartments providing support and cushioning are similar in structure to the fat pads of the foot, which simultaneously provide both firm support and progressive cushioning.

Existing cushioning systems cannot provide both firm support and progressive cushioning without also obstructing the natural pronation and supination motion of the foot, because the overall conception on which they are based is inherently flawed. The two most commercially successful proprietary systems are Nike Air, based on U.S. Pat. No. 4,219,945 issued Sep. 2, 1980, U.S. Pat. No. 4,183,156 issued Sep. 15, 1980, U.S. Pat. No. 4,271,606 issued Jun. 9, 1981, and U.S. Pat. No. 4,340,626 issued Jul. 20, 1982; and Asics Gel, based on U.S. Pat. No. 4,768,295 issued Sep. 6, 1988. Both of these cushioning systems and all of the other less popular ones have two essential flaws.

First, all such systems suspend the upper surface of the shoe sole directly under the important structural elements of the foot, particularly the critical heel bone, known as the calcaneus, in order to cushion it. That is, to provide good cushioning and energy return, all such systems support the foot's bone structures in buoyant manner, as if floating on a water bed or bouncing on a trampoline. None provide firm, direct structural support to those foot support structures; the shoe sole surface above the cushioning system never comes

in contact with the lower shoe sole surface under routine loads, like normal weight-bearing. In existing cushioning systems, firm structural support directly under the calcaneus and progressive cushioning are mutually incompatible. In marked contrast, it is obvious with the simplest tests that the barefoot is provided by very firm direct structural support by the fat pads underneath the bones contacting the sole, while at the same time it is effectively cushioned, though this Property is underdeveloped in habitually shoe shod feet.

Second, because such existing proprietary cushioning systems do not provide adequate control of foot motion or stability, they are generally augmented with rigid structures on the sides of the shoe uppers and the shoe soles, like heel counters and motion control devices, in order to provide control and stability. Unfortunately, these rigid structures seriously obstruct natural pronation and supination motion and actually increase lateral instability, as noted in the applicant's pending U.S. applications Ser. No. 07/219,387, filed on Jul. 15, 1988; U.S. Ser. No. 07/239,667, filed on Sep. 2, 1988; U.S. Ser. No. 07/400,714, filed on Aug. 30, 1989; U.S. Ser. No. 07/416,478, filed on Oct. 3, 1989; and U.S. Ser. No. 07/424,509, filed on Oct. 20, 1989, as well as in PCT application No. PCT/US89/03076 filed on Jul. 14, 1989. The purpose of the inventions disclosed in these applications was primarily to provide a neutral design that allows for natural foot and ankle biomechanics as close as possible to that between the foot and the ground, and to avoid the serious interference with natural foot and ankle biomechanics inherent in existing shoes.

In marked contrast to the rigid-sided proprietary designs discussed above, the barefoot provides stability at it sides by putting those sides, which are flexible and relatively inelastic, under extreme tension caused by the pressure of the compressed fat pads; they thereby become temporarily rigid when outside forces make that rigidity appropriate, producing none of the destabilizing lever arm torque problems of the permanently rigid sides of existing designs.

The applicant's '302 invention simply attempts, as closely as possible, to replicate the naturally effective structures of the foot that provide stability, support, and cushioning.

Accordingly, it was a general object of the '302 invention to elaborate upon the application of the principle of the natural basis for the support, stability and cushioning of the barefoot to shoe structures.

It was still another object of the '302 invention to provide a shoe having a sole with natural stability provided by attaching a completely flexible but relatively inelastic shoe sole upper directly to the bottom sole, enveloping the sides of the midsole, to put the side of the shoe upper under tension in reaction to destabilizing sideways forces on a tilting shoe.

It was still another object of the '302 invention to have that tension force is balanced and in equilibrium because the bottom sole is firmly anchored by body weight, so the destabilizing sideways motion is neutralized by the tension in the sides of the shoe upper.

It was another object of the '302 invention to create a shoe sole with support and cushioning which is provided by shoe sole compartments, filled with a pressure-transmitting medium like liquid, gas, or gel, that are similar in structure to the fat pads of the foot, which simultaneously provide both firm support and progressive cushioning.

These and other objects of the invention will become apparent from a detailed description of the invention which follows taken with the accompanying drawings.

BRIEF SUMMARY OF THE INVENTION

In its simplest conceptual form, the applicant's invention is the structure of a conventional shoe sole that has been modified by having its sides bent up so that their inner surface conforms to a shape nearly identical but slightly smaller than the shape of the outer surface of the foot sole of the wearer (instead of the shoe sole sides being flat on the ground, as is conventional). This concept is like that described in FIG. 3 of the applicant's Ser. No. 07/239,667 application; for the applicant's fully contoured design described in FIG. 15 of the '667 application, the entire shoe sole—including both the sides and the portion directly underneath the foot—is bent up to conform to a shape nearly identical but slightly smaller than the contoured shape of the unloaded foot sole of the wearer, rather than the partially flattened load-bearing foot sole shown in FIG. 3.

This theoretical or conceptual bending up must be accomplished in practical manufacturing without any of the puckering distortion or deformation that would necessarily occur if such a conventional shoe sole were actually bent up simultaneously along all of its the sides; consequently, manufacturing techniques that do not require any bending up of shoe sole material, such as injection molding manufacturing of the shoe sole, would be required for optimal results and therefore is preferable.

It is critical to the novelty of this fundamental concept that all layers of the shoe sole are bent up around the foot sole. A small number of both street and athletic shoe soles that are commercially available are naturally contoured to a limited extent in that only their bottom soles, which are about one quarter to one third of the total thickness of the entire shoe sole, are wrapped up around portions of the wearers' foot soles; the remaining soles layers, including the insole, midsole and heel lift (or heel) of such shoe soles, constituting over half of the thickness of the entire shoe sole, remains flat, conforming to the ground rather than the wearers' feet. (At the other extreme, some shoes in the existing art have flat midsoles and bottom soles, but have insoles that conform to the wearer's foot sole.)

Consequently, in existing contoured shoe soles, the total shoe sole thickness of the contoured side portions, including every layer or portion, is much less than the total thickness of the sole portion directly underneath the foot, whereas in the applicant's shoe sole inventions the shoe sole thickness of the contoured side portions are the same as or at least similar to the thickness of the sole portion directly underneath the foot.

This major and conspicuous structural difference between the applicant's underlying concept and the existing shoe sole art is paralleled by a similarly dramatic functional difference between the two: the aforementioned equivalent or similar thickness of the applicant's shoe sole invention maintains intact the firm lateral stability of the wearer's foot, that stability as demonstrated when the foot is unshod and tilted out laterally in inversion to the extreme limit of the normal range of motion of the ankle joint of the foot. The sides of the applicant's shoe sole invention extend sufficiently far up the sides of the wearer's foot sole to maintain the lateral stability of the wearer's foot when bare.

In addition, the applicant's shoe sole invention maintains the natural stability and natural, uninterrupted motion of the wearer's foot when bare throughout its normal range of sideways pronation and supination motion occurring during all load-bearing phases of locomotion of the wearer, including when the wearer is standing, walking, jogging and running, even when the foot is tilted to the extreme limit of

that normal range, in contrast to unstable and inflexible conventional shoe soles, including the partially contoured existing art described above. The sides of the applicant's shoe sole invention extend sufficiently far up the sides of the wearer's foot sole to maintain the natural stability and uninterrupted motion of the wearer's foot when bare. The exact thickness and material density of the shoe sole, sides and their specific contour will be determined empirically for individuals and groups using standard biomechanical techniques of gait analysis to determine those combinations that best provide the barefoot stability described above.

Finally, the shoe sole sides are sufficiently flexible to bend out easily when the shoes are put on the wearer's feet and therefore the shoe soles gently hold the sides of the wearer's foot sole when on, providing the equivalent of custom fit in a mass-produced shoe sole. In general, the applicant's preferred shoe sole embodiments include the structural and material flexibility to deform in parallel to the natural deformation of the wearer's foot sole as if it were bare and unaffected by any of the abnormal foot biomechanics created by rigid conventional shoe sole.

At the same time, the applicant's preferred shoe sole embodiments are sufficiently firm to provide the wearer's foot with the structural support necessary to maintain normal pronation and supination, as if the wearer's foot were bare; in contrast, the excessive softness of many of the shoe sole materials used in shoe soles in the existing art cause instability in the form of abnormally excessive foot pronation and supination.

Directed to achieving the aforementioned objects and to overcoming problems with prior art shoes, a shoe according to the '714 invention comprises a sole having at least a portion thereof following the contour of a theoretically ideal stability plane, and which further includes rounded edges at the finishing edge of the sole after the last point where the constant shoe sole thickness is maintained. Thus, the upper surface of the sole does not provide an unsupported portion that creates a destabilizing torque and the bottom surface does not provide an unnatural pivoting edge.

In another aspect in the '714 application, the shoe includes a naturally contoured sole structure exhibiting natural deformation which closely parallels the natural deformation of a foot under the same load. In a preferred embodiment, the naturally contoured side portion of the sole extends to contours underneath the load-bearing foot. In another embodiment, the sole portion is abbreviated alone its sides to essential support and propulsion elements wherein those elements are combined and integrated into the same discontinuous shoe sole structural elements underneath the foot, which approximate the principal structural elements of a human foot and their natural articulation between elements. The density of the abbreviated shoe sole can be treater than the density of the material used in an unabbreviated shoe sole to compensate for increased pressure loading. The essential support elements include the base and lateral tuberosity of the calcaneus, heads of the metatarsal, and the base of the fifth metatarsal.

The '714 application shoe sole is naturally contoured paralleling the shape of the foot in order to parallel its natural deformation, and made from a material which, when under load and tilting to the side, deforms in a manner which closely parallels that of the foot of its wearer, while retaining nearly the same amount of contact of the shoe sole with the ground as in its upright state under load. A deformable shoe sole according to the invention may have its sides bent inwardly somewhat so that when worn the sides bend out easily to approximate a custom fit.

Directed to achieving the aforementioned objects and to overcoming problems with prior art shoes, a shoe according to the '478 invention comprises a sole having at least a portion thereof following approximately the contour of a theoretically ideal stability plane, preferably applied to a naturally contoured shoe sole approximating the contour of a human foot.

In another aspect of the '478 invention, the shoe includes a naturally contoured sole structure exhibiting natural deformation which closely parallels the natural deformation of a foot under the same load, and having a contour which approximates, but increases beyond the theoretically ideal stability plane. When the shoe sole thickness is increased beyond the theoretically ideal stability plane, greater than natural stability results; when thickness is decreased, greater than natural motion results.

In a preferred embodiment of the '478 invention, such variations are consistent through all frontal plane cross sections so that there are proportionally equal increases to the theoretically ideal stability plane from front to back. In alternative embodiments, the thickness may increase, then decrease at respective adjacent locations, or vary in other thickness sequences. The thickness variations may be symmetrical on both sides, or asymmetrical, particularly since it may be desirable to provide greater stability for the medial side than the lateral side to compensate for common pronation problems. The variation pattern of the right shoe can vary from that of the left shoe. Variation in shoe sole density or bottom sole tread can also provide reduced but similar effects.

These and other features of the invention will become apparent from the detailed description of the invention which follows.

BRIEF DESCRIPTION OF THE DRAWINGS

FIGS. 1 through 9 are from prior copending applications of the applicant, with some new textual specification added. FIGS. 1–3 are from the '714 application; FIGS. 4–8 are from the '478 application; and FIG. 9 is from the '302 application.

FIGS. 1A to 1C [8] illustrate functionally the principles of natural deformation as applied to the shoe soles of the '667 and '714 invention.

FIG. 2 [9] shows variations in the relative density of the shoe sole including the shoe insole to maximize an ability of the sole to deform naturally.

FIG. 3 [10] shows a shoe having naturally contoured sides bent inwardly somewhat from a normal size so then when worn the shoe approximates a custom fit.

FIG. 4 shows a frontal plane cross section at the heel portion of a shoe with naturally contoured sides like those of FIG. 24, wherein a portion of the shoe sole thickness is increased beyond the theoretically ideal stability plane.

FIG. 5 is a view similar to FIG. 4, but of a shoe with fully contoured sides wherein the sole thickness increases with increasing distance from the center line of the ground-engaging portion of the sole.

FIG. 6 [10] is a view similar to FIGS. 29 and 30 showing still another density variation, one which is asymmetrical.

FIG. 7 [14] shows an embodiment like FIG. 25 but wherein a portion of the shoe sole thickness is decreased to less than the theoretically ideal stability plane.

FIG. 8 [13] shows a bottom sole tread design that provides a similar density variation as that in FIG. 6.

FIG. 9 [9] is the applicant's new shoe sole design in a sequential series of frontal plane cross sections of the heel at the ankle joint area that corresponds exactly to the FIG. 42 series below.

FIG. 10 is the applicant's custom fit design utilizing downsized flexible contoured shoe sole sides in combination with a thickness greater than the theoretically ideal stability plane.

FIG. 11 is the same custom fit design in combination with shoe sole side portions having a material with greater density than the sole portion.

FIGS. 12–23 are from the '714 application.

FIG. 12 [1] is a rear view of a heel of a foot for explaining the use of a stationery sprain simulation test.

FIG. 13 [2] is a rear view of a conventional running shoe unstably rotating about an edge of its sole when the shoe sole is tilted to the outside.

FIG. 14 [3] is a diagram of the forces on a foot when rotating in a shoe of the type shown in FIG. 2.

FIG. 15 [4] is a view similar to FIG. 3 but showing further continued rotation of a foot in a shoe of the type shown in FIG. 2.

FIG. 16 [5] is a force diagram during rotation of a shoe having motion control devices and heel counters.

FIG. 17 [6] is another force diagram during rotation of a shoe having a constant shoe sole thickness, but producing a destabilizing torque because a portion of the upper sole surface is unsupported during rotation.

FIG. 18 [7] shows an approach for minimizing destabilizing torque by providing only direct structural support and by rounding edges of the sole and its outer and inner surfaces.

FIG. 19 [11] shows a shoe sole having a fully contoured design but having sides which are abbreviated to the essential structural stability and propulsion elements that are combined and integrated into discontinuous structural elements underneath the foot that simulate those of the foot.

FIG. 20 [12] is a diagram serving as a basis for an expanded discussion of a correct approach for measuring shoe sole thickness.

FIG. 21 [13] shows several embodiments wherein the bottom sole includes most or all of the special contours of the new designs and retains a flat upper surface.

FIG. 22 [14], in FIGS. 22A–22C, show frontal plane cross sections of an enhancement to the previously-described embodiment.

FIG. 23 [15] shows, in FIGS. 23A–23C, the enhancement of FIG. 39 applied to the naturally contoured sides embodiment of the invention.

FIGS. 24–34 are from the '478 application.

FIG. 24 [1] shows, in frontal plane cross section at the heel portion of a shoe, the applicant's prior invention of a shoe sole with naturally contoured sides based on a theoretically ideal stability plane.

FIG. 25 [2] shows, again in frontal plane cross section, the most general case of the applicant's prior invention, a fully contoured shoe sole that follows the natural contour of the bottom of the foot as well as its sides, also based on the theoretically ideal stability plane.

FIG. 26 [3], as seen in FIGS. 26A to 26C in frontal plane cross section at the heel, shows the applicant's prior invention for conventional shoes, a quadrant-sided shoe sole, based on a theoretically ideal stability plane.

FIG. 27 [6] is a view similar to FIG. 5 where the fully contoured sole thickness variations are continually increasing on each side.

FIG. 28 [7] is a view similar to FIGS. 4, 5 & 27 wherein the sole thicknesses vary in diverse sequences.

FIG. 29 [8] is a frontal plane cross section showing a density variation in the midsole.

FIG. 30 [9] is a view similar to FIG. 29 wherein the firmest density material is at the outermost edge of the midsole contour.

FIG. 31 [11] shows a variation in the thickness of the sole for the quadrant embodiment which is greater than a theoretically ideal stability plane.

FIG. 32 [12] shows a quadrant embodiment as in FIG. 31 wherein the density of the sole varies.

FIG. 33 [14] shows embodiments like FIGS. 24 through 26 but wherein a portion of the shoe sole thickness is decreased to less than the theoretically ideal stability plane.

FIG. 34 [15] show embodiments with sides both greater and lesser than the theoretically ideal stability plane.

FIGS. 35–44 are from the '302 application.

FIG. 35 [1] is a perspective view of a typical athletic shoe for running known to the prior art to which the invention is applicable.

FIG. 36 [2] illustrates in a close-up frontal plane cross section of the heel at the ankle joint the typical shoe of existing art, undeformed by body weight, when tilted sideways on the bottom edge.

FIG. 37 [3] shows, in the same close-up cross section as FIG. 2, the applicant's prior invention of a naturally contoured shoe sole design, also tilted out.

FIG. 38 [4] shows a rear view of a barefoot heel tilted laterally 20 degrees.

FIG. 39 [5] shows, in a frontal plane cross section at the ankle joint area of the heel, the applicant's new invention of tension stabilized sides applied to his prior naturally contoured shoe sole.

FIG. 40 [6] shows, in a frontal plane cross section close-up, the FIG. 5 design when tilted to its edge, but undeformed by load.

FIG. 41 [7] shows, in frontal plane cross section at the ankle joint area of the heel, the FIG. 5 design when tilted to its edge and naturally deformed by body weight, though constant shoe sole thickness is maintained undeformed.

FIG. 42 [8] is a sequential series of frontal plane cross sections of the barefoot heel at the ankle joint area. FIG. 8A is unloaded and upright; FIG. 8B is moderately loaded by full body weight and upright. FIG. 8C is heavily loaded at peak landing force while running and upright; and FIG. 8D is heavily loaded and tilted out laterally to its about 20 degree maximum.

FIG. 43 [9] is the applicant's new shoe sole design in a sequential series of frontal plane cross sections of the heel at the ankle joint area that corresponds exactly to the FIG. 8 series above.

FIG. 44 [10] is two perspective views and a close-up view of the structure of fibrous connective tissue of the groups of fat cells of the human heel. FIG. 10A shows a quartered section of the calcaneus and the fat pad chambers below it; FIG. 10B shows a horizontal plane close-up of the inner structures of an individual chamber; and FIG. 10D shows a horizontal section of the whorl arrangement of fat pad underneath the calcaneus.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

FIGS. 1A–C illustrate, in frontal or transverse plane cross sections in the heel area, the applicant's concept of the theoretically ideal stability plane applied to shoe soles.

FIGS. 1A–1C illustrate clearly the principle of natural deformation as it applies to the applicant's design, even though design diagrams like those preceding (and in his previous applications already referenced) are normally shown in an ideal state, without any functional deformation, obviously to show their exact shape for proper construction. That natural structural shape, with its contour paralleling the foot, enables the shoe sole to deform naturally like the foot. In the applicant's invention, the natural deformation feature creates such an important functional advantage it will be illustrated and discussed here fully. Note in the figures that even when the shoe sole shale is deformed, the constant shoe sole thickness in the frontal plane feature of the invention is maintained.

FIG. 1A is FIG. 8A in the applicant's U.S. patent application Ser. No. 07/400,714 and FIG. 15 in his Ser. No. 07/239,667 application. FIG. 1A shows a fully contoured shoe sole design that follows the natural contour of all of the foot sole, the bottom as well,as the sides. The fully contoured shoe sole assumes that the resulting slightly rounded bottom when unloaded will deform under load as shown in FIG. 1B and flatten just as the human foot bottom is slightly round unloaded but flattens under load. Therefore, the shoe sole material must be of such composition as to allow the natural deformation following that of the foot. The design applies particularly to the heel, but to the rest of the shoe sole as well. By providing the closes match to the natural shape of the foot, the fully contoured design allows the foot to function as naturally as possible. Under load, FIG. 1A would deform by flattening to look essentially like FIG. 1B.

FIGS. 1A and 1B show in frontal plane cross section the essential concept underlying this invention, the theoretically ideal stability plane which is also theoretically ideal for efficient natural motion of all kinds, including running, jogging or walking. For any given individual, the theoretically ideal stability plane 51 is determined, first, by the desired shoe sole thickness (s) in a frontal plane cross section, and, second, by the natural shape of the individual's foot surface 29.

For the case shown in FIG. 1B, the theoretically ideal stability plane for any particular individual (or size average of individuals) is determined, first, by the given frontal plane cross section shoe sole thickness (s); second, by the natural shape of the individual's foot; and, third, by the frontal plane cross section width of the individual's load-bearing footprint which is defined as the supper surface of the shoe sole that is in physical contact with and supports the human foot sole.

FIG. 1B is FIG. 8B of the '714 application and shows the same fully contoured design when upright, under normal load (body weight) and therefore deformed naturally in a manner very closely paralleling the natural deformation under the same load of the foot. An almost identical portion of the foot sole that is flattened in deformation is also flatten in deformation in the shoe sole. FIG. 1C is FIG. 8C of the '714 application and shows the same design when tilted outward 20 degrees laterally, the normal barefoot limit; with virtually equal accuracy it shows the opposite foot tilted 20 degrees inward, in fairly severe pronation. As shown, the deformation of the shoe sole 28 again very closely parallels that of the foot, even as it tilts. Just as the area of foot contact is almost as great when tilted 20 degrees, the flattened area of the deformed shoe sole is also nearly the same as when upright. Consequently, the barefoot fully supported structurally and its natural stability is maintained undiminished, regardless of shoe tilt. In marked contrast, a conventional

shoe, shown in FIG. 12, makes contact with the around with only its relatively share edge when tilted and is therefore inherently unstable.

The capability to deform naturally is a design feature of the applicant's naturally contoured shoe sole designs, whether fully contoured or contoured only at the sides, though the fully contoured design is most optimal and is the most natural, general case, as note in the referenced Sep. 2, 1988, application, assuming shoe sole material such as to allow natural deformation. It is an important feature because, by following the natural deformation of the human foot, the naturally deforming shoe sole can avoid interfering with the natural biomechanics of the foot and ankle.

FIG. 1C also represents with reasonable accuracy a shoe sole design corresponding to FIG. 1B, a naturally contoured shoe sole with a conventional built-in flattening deformation, as in FIG. 14 of the above referenced Sep. 2, 1988, application, except that design would have a slight crime at 145. Seen in this light, the naturally contoured side design in FIG. 1B is a more conventional, conservative design that is a special case of the more generally fully contoured design in FIG. 1A, which is the closest to the natural form of the foot, but the least conventional.

In its simplest conceptual form, the applicant's FIG. 1 invention is the structure of a conventional shoe sole that has been modified by having its sides bent up so that their inner surface conforms to the shape of the outer surface of the foot sole of the wearer (instead of the shoe sole sides being flat on the ground, as is conventional); this concept is like that described in FIG. 3 of the applicant's Ser. No. 07/239,667 application. For the applicant's fully contoured design, the entire shoe sole—including both the sides and the portion directly underneath the foot—is bent up to conform to the shape of the unloaded foot sole, of the wearer, rather than the partially flattened load-bearing foot sole shown in FIG. 3.

This theoretical or conceptual bending up must be accomplished in practical manufacturing without any of the puckering distortion or deformation that would necessarily occur if such a conventional shoe sole were actually bent up simultaneously along all of its the sides; consequently, manufacturing techniques that do not require any bending up of shoe sole material, such as injection molding manufacturing of the shoe sole, would be required for optimal results and therefore is preferable.

It is critical to the novelty of this fundamental concept that all layers of the shoe sole are bent up around the foot sole. A small number of both street and athletic shoe soles that are commercially available are naturally contoured to a limited extent in that only their bottom soles, which are about one quarter to one third of the total thickness of the entire shoe sole, are wrapped up around portions of the wearersg foot soles; the remaining sole layers, including the insole, the midsole and the heel lift (or heel) of such shoe soles, constituting over half of the thickness of the entire shoe sole, remains flat, conforming to the ground rather than the wearers' feet.

Consequently, in existing contoured shoe soles, the shoe sole thickness of the contoured side portions is much less than the thickness of the sole portion directly underneath the foot, whereas in the applicant's shoe sole inventions the shoe sole thickness of the contoured side portions are the same as the thickness of the sole portion directly underneath the foot.

This major and conspicuous structural difference between the applicant's underlying concept and the existing shoe sole art is paralleled by a similarly dramatic functional difference between the two: the aforementioned equivalent or similar thickness of the applicant's shoe sole invention maintains

intact the firm lateral stability of the wearer's foot, as demonstrated when the foot is unshod and tilted out laterally in inversion to the extreme limit of the normal range of motion of the ankle joint of the foot; in a similar demonstration in a conventional shoe sole, the wearer's foot and ankle are unstable. The sides of the applicant's shoe sole invention extend sufficiently far up the sides of the wearer's foot sole to maintain the lateral stability of the wearer's foot when bare.

In addition, the applicant's shoe sole invention maintains the natural stability and natural, uninterrupted motion of the wearer's foot when bare throughout its normal range of sideways pronation and supination motion occurring during all load-bearing phases of locomotion of the wearer, including when said wearer is standing, walking, jogging and running, even when said foot is tilted to the extreme limit of that normal range, in contrast to unstable and inflexible conventional shoe soles, including the partially contoured existing art described above. The sides of the applicant's shoe sole invention extend sufficiently far up the sides of the wearer's foot sole to maintain that natural stability and uninterrupted motion.

For the FIG. 1 shoe sole invention, the amount of any shoe sole side portions coplanar with the theoretically ideal stability plane is determined by the degree of shoe sole stability desired and the shoe sole weight and bulk required to provide said stability; the amount of said coplanar contoured sides that is provided said shoe sole being sufficient to maintain intact the firm stability of the wearer's foot throughout the range of foot inversion and eversion motion typical of the use for which the shoe is intended and also typical of the kind of wearer—such as normal or excessive pronator—for which said shoe is intended.

As mentioned earlier, FIG. 1A is FIG. 15 in the applicant's Ser. No. 07/239,667 application; however, it does not show the heel lift 38 which is included in the original FIG. 15. That heel lift is shown with constant frontal or transverse plane thickness, since it is oriented conventionally in alignment with the frontal or transverse plane and perpendicular to the long axis of the shoe sole; consequently, the thickness of the heel lift decreases uniformly in the frontal or transverse plane between the heel and the forefoot when moving forward along the long axis of the shoe sole. However, the conventional heel wedge, or toe taper or other shoe sole thickness variations in the sagittal plane along the long axis of the shoe sole, can be located at an angle to the conventional alignment.

For example, the heel wedge can be rotated inward in the horizontal plane so that it is located perpendicular to the subtalar axis, which is located in the heel area generally about 20 to 25 degrees medially, although a different angle can be used base on individual or group testing; such a orientation may provide better, more natural support to the subtalar joint, through which critical pronation and supination motion occur. The applicant's theoretically ideal stability plane concept would teach that such a heel wedge orientation would require constant shoe sole thickness in a vertical plane perpendicular to the chosen subtalar joint axis, instead of the frontal plane.

FIG. 2 is FIG. 9 of the '714 application and shows, in frontal or transverse plane cross section in the heel area, the preferred relative density of the shoe sole, including the insole as a part, order to maximize the shoe sole's ability to deform naturally following the natural deformation of the foot sole. Regardless of how many shoe sole layers (including insole) or laminations of differing material densities and flexibility are used in total, the softest and most flexible

material 147 should be closest to the foot sole, with a progression through less soft 148 to the firmest and least flexible 149 at the outermost shoe sole layer, the bottom sole. This arrangement helps to avoid the unnatural side lever arm/torque problem mentioned in the previous several figures.

FIG. 3, which is a frontal or transverse plane cross section at the heel, is FIG. 10 from the applicant's copending U.S. patent application Ser. No. 07/400,714, filed Aug. 30, 1989. FIG. 3 illustrates that the applicant's naturally contoured shoe sole sides can be made to provide a fit so close as to approximate a custom fit. By molding each mass-produced shoe size with sides that are bent in somewhat from the position 29 they would normally be in to conform to that standard size shoe last, the shoe soles so produced will very gently hold the sides of each individual foot exactly. Since the shoe sole is designed as described in connection with FIG. 2 (FIG. 9 of the applicant's copending application Ser. No. 07/400,714) to deform easily and naturally like that of the bare foot, it will deform easily to provide this designed-in custom fit. The greater the flexibility of the shoe sole sides, the greater the range of individual foot size. This approach applies to the fully contoured design described here in FIG. 1A (FIG. 8A of the '714 application) and in FIG. 15, U.S. patent application Ser. No. 07/239,667 (filed 02 Sep. 1988), as well, which would be even more effective than the naturally contoured sides design shown in FIG. 3.

Besides providing a better fit, the intentional undersizing of the flexible shoe sole sides allows for simplified design of shoe sole lasts, since they can be designed according to the simple geometric methodology described in the textual specification of FIG. 27, U.S. application Ser. No. 07/239, 667 (filed 02 Sep. 1988). That geometric approximation of the true actual contour of the human is close enough to provide a virtual custom fit, when compensated for by the flexible undersizing from standard shoe lasts described above.

Expanding on the '714 application, a flexible undersized version of the fully contoured design described in FIG. 1A (and 8A of the '714 application) can also be provided by a similar geometric approximation. As a result, the undersized flexible shoe sole sides allow the applicant's shoe sole inventions based on the theoretically ideal stability plane to be manufactured in relatively standard sizes in the same manner as are shoe uppers, since the flexible shoe sole sides can be built on standard shoe lasts, even though conceptually those sides conform closely to the specific shape of the individual wearer's foot sole, because the flexible sides bend to conform when on the wearer's foot sole.

FIG. 3 shows the shoe sole structure when not on the foot of the wearer; the dashed line 29 indicates the position of the shoe last, which is assumed to be a reasonably accurate approximation of the shape of the outer surface of the wearer's foot sole, which determines the shape of the theoretically ideal stability plane 51. Thus, the dashed lines 29 and 51 show what the positions of the inner surface 30 and outer surface 31 of the shoe sole would be when the shoe is put on the foot of the wearer. Numbering with the figures in this application is consistent with the numbering used in prior applications of the applicant.

The FIG. 3 invention provides a way make the inner surface 30 of the contoured shoe sole, especially its sides, conform very closely to the outer surface 29 of the foot sole of a wearer. It thus makes much more practical the applicant's earlier underlying naturally contoured designs shown in FIGS. 1A–C. The shoe sole structures shown in FIG. 1, then, are what the FIG. 3 shoe sole structure would be when

on the wearer's foot, where the inner surface **30** of the shoe upper is bent out to virtually coincide with the outer surface of the foot sole of the wearer **29** (the figures in this and prior applications show one line to emphasize the conceptual coincidence of what in fact are two lines; in real world embodiments, some divergence of the surface, especially under load and during locomotion would be unavoidable).

In its simplest conceptual form, the applicant's invention is the structure of a conventional shoe sole that has been modified by having its sides bent up so that their inner surface conforms to a shape nearly identical but slightly smaller than the shape of the outer surface of the foot sole of the wearer (instead of the shoe sole sides being flat on the ground, as is conventional); this concept is like that described in FIG. **3** of the applicant's Ser. No. 07/239,667 application. For the applicant's fully contoured design described in FIG. **15** of the '667 application, the entire shoe sole—including both the sides and the portion directly underneath the foot—is bent up to conform to a shape nearly identical but slightly smaller than the contoured shape of the unloaded foot sole of the wearer, rather than the partially flattened load-bearing foot sole shown in FIG. **3**.

This theoretical or conceptual bending up must be accomplished in practical manufacturing without any of the puckering distortion or deformation that would necessarily occur if such a conventional shoe sole were actually bent up simultaneously along all of its the sides; consequently, manufacturing techniques that do not require any bending up of shoe sole material, such as injection molding manufacturing of the shoe sole, would be required for optimal results and therefore is preferable.

It is critical to the novelty of this fundamental concept that all layers of the shoe sole are bent up around the foot sole. A small number of both street and athletic shoe soles that are commercially available are naturally contoured to a limited extent in that only their bottom soles, which are about one quarter to one third of the total thickness of the entire shoe sole, are wrapped up around portions of the wearers' foot soles; the midsole and heel lift (or heel) of such shoe soles, constituting over half of the thickness of the entire shoe sole, remains flat, conforming to the ground rather than the wearers' feet. (At the other extreme, some shoes in the existing art have flat midsoles and bottom soles, but have insoles that conform to the wearer's foot sole.)

Consequently, in existing contoured shoe soles, the shoe sole thickness of the contoured side portions is much less than the thickness of the sole portion directly underneath the foot, whereas in the applicant's shoe sole inventions the shoe sole thickness of the contoured side portions are the same as the thickness of the sole portion directly underneath the foot.

This major and conspicuous structural difference between the applicant's underlying concept and the existing shoe sole art is paralleled by a similarly dramatic functional difference between the two: the aforementioned equivalent thickness of the applicant's shoe sole invention maintains intact the firm lateral stability of the wearer's foot, as demonstrated when the foot is unshod and tilted out laterally in inversion to the extreme limit of the normal range of motion of the ankle joint of the foot; in a similar demonstration in a conventional shoe sole, the wearer's foot and ankle are unstable. The sides of the applicant's shoe sole invention extend sufficiently far up the sides of the wearer's foot sole to maintain the lateral stability of the wearer's foot when bare.

In addition, the applicant's shoe sole invention maintains the natural stability and natural, uninterrupted motion of the wearer's foot when bare throughout its normal range of sideways pronation and supination motion occurring during all load-bearing phases of locomotion of the wearer, including when the wearer is standing, walking, jogging and running, even when said foot is tilted to the extreme limit of that normal range, in contrast to unstable and inflexible conventional shoe soles, including the partially contoured existing art described above. The sides of the applicant's shoe sole invention extend sufficiently far up the sides of the wearer's foot sole to maintain the natural stability and uninterrupted motion of the wearer's foot when bare.

For the FIG. **3** shoe sole invention, the amount of any shoe sole side portions coplanar with the theoretically ideal stability plane is determined by the degree of shoe sole stability desired and the shoe sole weight and bulk required to provide said stability; the amount of said coplanar contoured sides that is provided said shoe sole being sufficient to maintain intact the firm stability of the wearer's foot throughout the range of foot inversion and eversion motion typical of the use for which the shoe is intended and also typical of the kind of wearer—such as normal or excessive pronator—for which said shoe is intended.

The shoe sole sides of the FIG. **3** invention are sufficiently flexible to bend out easily when the shoes are put on the wearer's feet and therefore the shoe soles gently hold the sides of the wearer's foot sole when on, providing the equivalent of custom fit in a mass-produced shoe sole. In general, the applicant's preferred shoe sole embodiments include the structural and material flexibility to deform in parallel to the natural deformation of the wearer's foot sole as if it were bare and unaffected by any of the abnormal foot biomechanics created by rigid conventional shoe sole.

At the same time, the applicant's preferred shoe sole embodiments are sufficiently firm to provide the wearer's foot with the structural support necessary to maintain normal pronation and supination, as if the wearer's foot were bare; in contrast, the excessive softness of many of the shoe sole materials used in shoe soles in the existing art cause abnormal foot pronation and supination.

FIG. **3** is a frontal or transverse plane cross section at the heel, so the structure is shown at one of the essential structural support and propulsion elements, as specified by applicant in his copending Ser. No. 07/239,667 application in its FIG. 21 specification. The essential structural support elements are the base and lateral tuberosity of the calcaneus **95**, the heads of the metatarsals **96**, and the base of the fifth metatarsal **97**; the essential propulsion element is the head of the first distal phalange **98**. The FIG. **3** shoe sole structure can be abbreviated along its sides to only the essential structural support and propulsion elements, like FIG. 21 of the '667 application. The FIG. **3** design can also be abbreviated underneath the shoe sole to the same essential structural support and propulsion elements, as shown in FIG. 28 of the '667 application.

As mentioned earlier regarding FIG. **1A**, the applicant has previously shown heel lifts with constant frontal or transverse plane thickness, since it is oriented conventionally in alignment with the frontal or transverse plane and perpendicular to the long axis of the shoe sole. However, the heel wedge (or toe taper or other shoe sole thickness variations in the sagittal plane along the long axis of the shoe sole) can be located at an angle to the conventional alignment in the FIG. **3** design.

For example, the heel wedge can be rotated inward in the horizontal plane so that it is located perpendicular to the subtalar axis, which is located in the heel area generally about 20 to 25 degrees medially, although a different angle can be used base on individual or group testing; such a orientation may provide better, more natural support to the

subtalar joint, through which critical pronation and supination motion occur. The applicant's theoretically ideal stability plane concept would teach that such a heel wedge orientation would require constant shoe sole thickness in a vertical plane perpendicular to the chosen subtalar joint axis, instead of the frontal plane.

The sides of the shoe sole structure described under FIG. 3 can also be used to form a slightly less optimal structure: a conventional shoe sole that has been modified by having its sides bent up so that their inner surface conforms to shape nearly identical but slightly larger than the shape of the outer surface of the foot sole of the wearer, instead of the shoe sole sides being flat on the ground, as is conventional. Clearly, the closer the sides are to the shape of the wearer's foot sole, the better as a general rule, but any side position between flat on the ground and conforming like FIG. 3 to a shape slightly smaller than the wearer's shape is both possible and more effective than conventional flat shoe sole sides. And in some cases, such as for diabetic patients, it may be optimal to have relatively loose shoe sole sides providing no conforming pressure of the shoe sole on the tender foot sole; in such cases, the shape of the flexible shoe uppers, which can even be made with very elastic materials such as lycra and spandex, can provide the capability for the shoe, including the shoe sole, to conform to the shape of the foot.

As discussed earlier by the applicant, the critical functional feature of a shoe sole is that it deforms under a weight-bearing load to conform to the foot sole just as the foot sole deforms to conform to the ground under a weight-bearing load. So, even though the foot sole and the shoe sole may start in different locations—the shoe sole sides can even be conventionally flat on the ground—the critical functional feature of both is that they both conform under load to parallel the shape of the ground, which conventional shoes do not, except when exactly upright. Consequently, the applicant's shoe sole invention, stated most broadly, includes any shoe sole—whether conforming to the wearer's foot sole or to the ground or some intermediate position, including a shape much smaller than the wearer's foot sole—that deforms to conform to the theoretically ideal stability plane, which by definition itself deforms in parallel with the deformation of the wearer's foot sole under weight-bearing load.

Of course, it is optimal in terms of preserving natural foot biomechanics, which is the primary goal of the applicant, for the shoe sole to conform to the foot sole when on the foot, not just when under a weight-bearing load. And, in any case, all of the essential structural support and propulsion elements previously identified by the applicant in discussing FIG. 3 must be supported by the foot sole.

To the extent the shoe sole sides are easily flexible, as has already been specified as desirable, the position of the shoe sole sides before the wearer puts on the shoe is less important, since the sides will easily conform to the shape of the wearer's foot when the shoe is put on that foot. In view of that, even shoe sole sides that conform to a shape more than slightly smaller than the shape of the outer surface of the wearer's foot sole would function in accordance with the applicant's general invention, since the flexible sides could bend out easily a considerable relative distance and still conform to the wearer's foot sole when on the wearer's foot.

FIG. 4 is FIG. 4 from the applicant's copending U.S. patent application Ser. No. 07/416,478, filed Oct. 3, 1989. FIG. 4 illustrates, in frontal or transverse plane cross section in the heel area, the applicant's new invention of shoe sole side thickness increasing beyond the theoretically ideal stability plane to increase stability somewhat beyond its

natural level. The unavoidable trade-off resulting is that natural motion would be restricted somewhat and the weight of the shoe sole would increase somewhat.

FIG. 4 shows a situation wherein the thickness of the sole at each of the opposed sides is thicker at the portions of the sole 31a by a thickness which gradually varies continuously from a thickness (s) through a thickness (s+s1), to a thickness (s+s2).

These designs recognize that lifetime use of existing shoes, the design of which has an inherent flaw that continually disrupts natural human biomechanics, has produced thereby actual structural changes in a human foot and ankle to an extent that must be compensated for. Specifically, one of the most common of the abnormal effects of the inherent existing flaw is a weakening of the long arch of the foot, increasing pronation. These designs therefore modify the applicant's preceding designs to provide greater than natural stability and should be particularly useful to individuals, generally with low arches, prone to pronate excessively, and could be used only on the medial side. Similarly, individuals with high arches and a tendency to over supinate and lateral ankle sprains would also benefit, and the design could be used only on the lateral side. A shoe for the general population that compensates for both weaknesses in the same shoe would incorporate the enhanced stability of the design compensation on both sides.

The new design in FIG. 4 (like FIGS. 1 and 2 of the '478 application) allows the shoe sole to deform naturally closely paralleling the natural deformation of the barefoot under load; in addition, shoe sole material must be of such composition as to allow the natural deformation following that of the foot.

The new designs retain the essential novel aspect of the earlier designs; namely, contouring the shape of the shoe sole to the shape of the human foot. The difference is that the shoe sole thickness in the frontal plane is allowed to vary rather than remain uniformly constant. More specifically, FIG. 4 (and FIGS. 5, 6, 7, and 11 of the '478 application) show, in frontal plane cross sections at the heel, that the shoe sole thickness can increase beyond the theoretically ideal stability plane 51, in order to provide greater than natural stability. Such variations (and the following variations) can be consistent through all frontal plane cross sections, so that there are proportionately equal increases to the theoretically ideal stability plane 51 from the front of the shoe sole to the back, or that the thickness can vary, preferably continuously, from one frontal plane to the next.

The exact amount of the increase in shoe sole thickness beyond the theoretically ideal stability plane is to be determined empirically. Ideally, right and left shoe soles would be custom designed for each individual based on an biomechanical analysis of the extent of his or her foot and ankle disfunction in order to provide an optimal individual correction. If epidemiological studies indicate general corrective patterns for specific categories of individuals or the population as a whole, then mass-produced corrective shoes with soles incorporating contoured sides exceeding the theoretically ideal stability plane would be possible. It is expected that any such mass-produced corrective shoes for the general population would have thicknesses exceeding the theoretically ideal stability plane by an amount up to 5 or 10 percent, while more specific groups or individuals with more severe disfunction could have an empirically demonstrated need for greater corrective thicknesses on the order of up to 25 percent more than the theoretically ideal stability plane. The optimal contour for the increased thickness may also be determined empirically.

As described in the '478 application, in its simplest conceptual form, the applicant's FIG. 4 invention is the structure of a conventional shoe sole that has been modified by having its sides bent up so that their inner surface conforms to a shape of the outer surface of the foot sole of the wearer (instead of the shoe sole sides conforming to the ground by paralleling it, as is conventional); this concept is like that described in FIG. 3 of the applicant's Ser. No. 07/239,667 application. For the applicant's fully contoured design described in FIG. 15 of the '667 application, the entire shoe sole—including both the sides and the portion directly underneath the foot—is bent up to conform to a shape nearly identical but slightly smaller than the contoured shape of the unloaded foot sole of the wearer, rather than the partially flattened load-bearing foot sole shown in FIG. 3.

This theoretical or conceptual bending up must be accomplished in practical manufacturing without any of the puckering distortion or deformation that would necessarily occur if such a conventional shoe sole were actually bent up simultaneously along all of its the sides; consequently, manufacturing techniques that do not require any bending up of shoe sole material, such as injection molding manufacturing of the shoe sole, would be required for optimal results and therefore is preferable.

It is critical to the novelty of this fundamental concept that all layers of the shoe sole are bent up around the foot sole. A small number of both street and athletic shoe soles that are commercially available are naturally contoured to a limited extent in that only their bottom soles, which are about one quarter to one third of the total thickness of the entire shoe sole, are wrapped up around portions of the wearers' foot soles; the midsole and heel lift (or heel) of such shoe soles, constituting over half of the thickness of the entire shoe sole, remains flat, conforming to the ground rather than the wearers' feet. (At the other extreme, some shoes in the existing art have flat midsoles and bottom soles, but have insoles that conform to the wearer's foot sole.)

Consequently, in existing contoured shoe soles, the shoe sole thickness of the contoured side portions is much less than the thickness of the sole portion directly underneath the foot, whereas in the applicant's shoe sole inventions the shoe sole thickness of the contoured side portions are the at least similar to the thickness of the sole portion directly underneath the foot.

This major and conspicuous structural difference between the applicant's underlying concept and the existing shoe sole art is paralleled by a similarly dramatic functional difference between the two: the aforementioned similar thickness of the applicant's shoe sole invention maintains intact the firm lateral stability of the wearer's foot, as demonstrated when the foot is unshod and tilted out laterally in inversion to the extreme limit of the normal range of motion of the ankle joint of the foot; in a similar demonstration in a conventional shoe sole, the wearer's foot and ankle are unstable. The sides of the applicant's shoe sole invention extend sufficiently far up the sides of the wearer's foot sole to maintain the lateral stability of the wearer's foot when bare.

In addition, the applicant's shoe sole invention maintains the natural stability and natural, uninterrupted motion of the wearer's foot when bare throughout its normal range of sideways pronation and supination motion occurring during all load-bearing phases of locomotion of the wearer, including when the wearer is standing, walking, jogging and running, even when said foot is tilted to the extreme limit of that normal range, in contrast to unstable and inflexible conventional shoe soles, including the partially contoured existing art described above. The sides of the applicant's

shoe sole invention extend sufficiently far up the sides of the wearer's foot sole to maintain the natural stability and uninterrupted motion of the wearer's foot when bare. The exact thickness of the shoe sole sides and their specific contour will be determined empirically for individuals and groups using standard biomechanical techniques of gait analysis to determine those combinations that best provide the barefoot stability described above.

For the FIG. 4 shoe sole invention, the amount of any shoe sole side portions coplanar with the theoretically ideal stability plane is determined by the degree of shoe sole stability desired and the shoe sole weight and bulk required to provide said stability; the amount of said coplanar contoured sides that is provided said shoe sole being sufficient to maintain intact the firm stability of the wearer's foot throughout the range of foot inversion and eversion motion typical of the use for which the shoe is intended and also typical of the kind of wearer—such as normal or excessive pronator—for which said shoe is intended.

In general, the applicant's preferred shoe sole embodiments include the structural and material flexibility to deform in parallel to the natural deformation of the wearer's foot sole as if it were bare and unaffected by any of the abnormal foot biomechanics created by rigid conventional shoe sole.

At the same time, the applicant's preferred shoe sole embodiments are sufficiently firm to provide the wearer's foot with the structural support necessary to maintain normal pronation and supination, as if the wearer's foot were bare; in contrast, the excessive softness of many of the shoe sole materials used in shoe soles in the existing art cause abnormal foot pronation and supination.

As mentioned earlier regarding FIG. 1A, the applicant has previously shown heel lifts with constant frontal or transverse plane thickness, since it is oriented conventionally in alignment with the frontal or transverse plane and perpendicular to the long axis of the shoe sole. However, the heel wedge (or toe taper or other shoe sole thickness variations in the sagittal plane along the long axis of the shoe sole) can be located at an angle to the conventional alignment in the FIG. 4 design.

For example, the heel wedge can be located perpendicular to the subtalar axis, which is located in the heel area generally about 20 to 25 degrees medially, although a different angle can be used base on individual or group testing; such a orientation may provide better, more natural support to the subtalar joint, through which critical pronation and supination motion occur. The applicant's theoretically ideal stability plane concept would teach that such a heel wedge orientation would require constant shoe sole thickness in a vertical plane perpendicular to the chosen subtalar joint axis, instead of the frontal plane.

FIG. 5 is FIG. 5 in the applicant's copending U.S. patent application Ser. No. 07/416,478 and shows, in frontal or transverse plane cross section in the heel area, a variation of the enhanced fully contoured design wherein the shoe sole begins to thicken beyond the theoretically ideal stability plane 51 somewhat offset to the sides.

FIG. 6 is FIG. 10 in the applicant's copending ['714] '478 application and shows, in frontal or transverse plane cross section in the heel area, that similar variations in shoe midsole (other portions of the shoe sole area not shown) density can provide similar but reduced effects to the variations in shoe sole thickness described previously in FIGS. 4 and 5. The major advantage of this approach is that the structural theoretically ideal stability plane is retained, so

that naturally optimal stability and efficient motion are retained to the maximum extent possible.

The ['714] '478 application showed midsole only, since that is where material density variation has historically been most common. Density variations can and do, of course, also occur in other layers of the shoe sole, such as the bottom sole and the inner sole, and can occur in any combination and in symmetrical or asymmetrical patterns between layers or between frontal or transverse plane cross sections.

The major and conspicuous structural difference between the applicant's underlying concept and the existing shoe sole art is paralleled by a similarly dramatic functional difference between the two: the aforementioned similar thickness of the applicant's shoe sole invention maintains intact the firm lateral stability of the wearer's foot, as demonstrated when the foot is unshod and tilted out laterally in inversion to the extreme limit of the normal range of motion of the ankle joint of the foot; in a similar demonstration in a conventional shoe sole, the wearer's foot and ankle are unstable. The sides of the applicant's shoe sole invention extend sufficiently far up the sides of the wearer's foot sole to maintain the lateral stability of the wearer's foot when bare.

In addition, the applicant's shoe sole invention maintains the natural stability and natural, uninterrupted motion of the wearer's foot when bare throughout its normal range of sideways pronation and supination motion occurring during all load-bearing phases of locomotion of the wearer, including when the wearer is standing, walking, jogging and running, even when said foot is tilted to the extreme limit of that normal range, in contrast to unstable and inflexible conventional shoe soles, including the partially contoured existing art described above. The sides of the applicant's shoe sole invention extend sufficiently far up the sides of the wearer's foot sole to maintain the natural stability and uninterrupted motion of the wearer's foot when bare. The exact material density of the shoe sole sides will be determined empirically for individuals and groups using standard biomechanical techniques of gait analysis to determine those combinations that best provide the barefoot stability described above.

For the FIG. 6 shoe sole invention, the amount of any shoe sole side portions coplanar with the theoretically ideal stability plane is determined by the degree of shoe sole stability desired and the shoe sole weight and bulk required to provide said stability; the amount of said coplanar contoured sides that is provided said shoe sole being sufficient to maintain intact the firm stability of the wearer's foot throughout the range of foot inversion and eversion motion typical of the use for which the shoe is intended and also typical of the kind of wearer—such as normal or excessive pronator—for which said shoe is intended.

In general, the applicant's preferred shoe sole embodiments include the structural and material flexibility to deform in parallel to the natural deformation of the wearer's foot sole as if it were bare and unaffected by any of the abnormal foot biomechanics created by rigid conventional shoe sole.

At the same time, the applicant's preferred shoe sole embodiments are sufficiently firm to provide the wearer's foot with the structural support necessary to maintain normal pronation and supination, as if the wearer's foot were bare; in contrast, the excessive softness of many of the shoe sole materials used in shoe soles in the existing art cause abnormal foot pronation and supination.

As mentioned earlier regarding FIG. 1A, the applicant has previously shown heel lifts with constant frontal or transverse plane thickness, since it is oriented conventionally in

alignment with the frontal or transverse plane and perpendicular to the long axis of the shoe sole. However, the heel wedge (or toe taper or other shoe sole thickness variations in the sagittal plane along the long axis of the shoe sole) can be located at an angle to the conventional alignment in the FIG. 4 design.

For example, the heel wedge can be located perpendicular to the subtalar axis, which is located in the heel area generally about 20 to 25 degrees medially, although a different angle can be used base on individual or group testing; such a orientation may provide better, more natural support to the subtalar joint, through is which critical pronation and supination motion occur. The applicants theoretically ideal stability plane concept would teach that such a heel wedge orientation would require constant shoe sole thickness in a vertical plane perpendicular to the chosen subtalar joint axis, instead of the frontal plane.

FIG. 7 is FIG. 14B of the applicant's ['714] '478 application and shows, in frontal or transverse plane cross sections in the heel area, embodiments like those in FIGS. 4 through 6 but wherein a portion of the shoe sole thickness is decreased to less than the theoretically ideal stability plane. It is anticipated that some individuals with foot and ankle biomechanics that have been degraded by existing shoes may benefit from such embodiments, which would provide less than natural stability but greater freedom and motion, and less shoe sole weight and bulk. FIG. 7 shows a embodiment like the fully contoured design in FIG. 5, but with a show sole thickness decreasing with increasing distance from the center portion of the sole.

FIG. 8 is FIG. 13 of the ['714] '478 application and shows, in frontal or transverse plane cross section, a bottom sole tread design that provides about the same overall shoe sole density variation as that provided in FIG. 6 by midsole density variation. The less supporting tread there is under any particular portion of the shoe sole, the less effective overall shoe density there is, since the midsole above that portion will deform more easily than if it were fully supported.

FIG. 8 from the ['714] '478 is illustrative of the applicant's point that bottom sole tread patterns, just like midsole or bottom sole or inner sole density, directly affect the actual structural support the foot receives from the shoe sole. Not shown, but a typical example in the real world, is the popular "center of pressure" tread pattern, which is like a backward horseshoe attached to the heel that leaves the heel area directly under the calcaneus unsupported by tread, so that all of the weight bearing load in the heel area is transmitted to outside edge treads. Variations of this pattern are extremely common in athletic shoes and are nearly universal in running shoes, of which the 1991 Nike 180 model and the Avia "cantilever" series are examples.

The applicant's ['714] '478 shoe sole invention can, therefore, utilize bottom sole tread patterns like any these common examples, together or even in the absence of any other shoe sole thickness or density variation, to achieve an effective thickness greater than the theoretically ideal stability plane, in order to achieve greater stability than the shoe sole would otherwise provide, as discussed earlier under FIGS. 4–6.

The applicant's shoe sole invention maintains intact the firm lateral stability of the wearer's foot, that stability as demonstrated when the foot is unshod and tilted out laterally in inversion to the extreme limit of the normal range of motion of the ankle joint of the foot. The sides of the applicant's shoe sole invention extend sufficiently far up the

sides of the wearer's foot sole to maintain the lateral stability of the wearer's foot when bare.

In addition, the applicant's shoe sole invention maintains the natural stability and natural, uninterrupted motion of the wearer's foot when bare throughout its normal range of sideways pronation and supination motion occurring during all load-bearing phases of locomotion of the wearer, including when the wearer is standing, walking, jogging and running, even when the foot is tilted to the extreme limit of that normal range, in contrast to unstable and inflexible conventional shoe soles, including the partially contoured existing art described above. The sides of the applicant's shoe sole invention extend sufficiently far up the sides of the wearer's foot sole to maintain the natural stability and uninterrupted motion of the wearer,s foot when bare. The exact thickness and material density of the bottom sole tread, as well as the shoe sole sides and their specific contour, will be determined empirically for individuals and groups using standard biomechanical techniques of gait analysis to determine those combinations that best provide the barefoot stability described above.

FIG. 9 is FIG. 9A from the applicant's copending U.S. patent application Ser. No. 07/463,302, filed Jan. 10, 1990. FIG. 9A shows, also in cross sections at the heel, a naturally contoured shoe sole design that parallels as closely as possible the overall natural cushioning and stability system of the barefoot (described in FIG. 8 of the '302 application), including a cushioning compartment 161 under support structures of the foot containing a pressure-transmitting medium like gas, gel, or liquid, like the subcalcaneal fat pad under the calcaneus and other bones of the foot; consequently, FIGS. 9A–D from '302, shown completely in FIGS. 43A–D in this application, directly correspond to FIGS. 8A–D of '302, shown as FIGS. 42A–D in this application. The optimal pressure-transmitting medium is that which most closely approximates the fat pads of the foot; silicone gel is probably most optimal of materials currently readily available, but future improvements are probable; since it transmits pressure indirectly, in that it compresses in volume under pressure, gas is significantly less optimal. The gas, gel, or liquid, or any other effective material, can be further encapsulated itself, in addition to the sides of the shoe sole, to control leakage and maintain uniformity, as is common conventionally, and can be subdivided into any practical number of encapsulated areas within a compartment, again as is common conventionally. The relative thickness of the cushioning compartment 161 can vary, as can the bottom sole 149 and the upper midsole 147, and can be consistent or differ in various areas of the shoe sole; the optimal relative sizes should be those that approximate most closely those of the average human foot, which suggests both smaller upper and lower soles and a larger cushioning compartment than shown in FIG. 9. And the cushioning compartments or pads 161 can be placed anywhere from directly underneath the foot, like an insole, to directly above the bottom sole. Optimally, the amount of compression created by a given load in any cushioning compartment 161 should be tuned to approximate as closely as possible the compression under the corresponding fat pad of the foot.

The function of the subcalcaneal fat pad is not met satisfactorily with existing proprietary cushioning systems, even those featuring gas, gel or liquid as a pressure transmitting medium. In contrast to those artificial systems, the new design shown is FIG. 9 conforms to the natural contour of the foot and to the natural method of transmitting bottom pressure into side tension in the flexible but relatively

non-stretching (the actual optimal elasticity will require empirical studies) sides of the shoe sole.

Existing cushioning systems like Nike Air or Asics Gel do not bottom out under moderate loads and rarely if ever do so even partially under extreme loads; the upper surface of the cushioning device remains suspended above the lower surface. In contrast, the new design in FIG. 9 provides firm support to foot support structures by providing for actual contact between the lower surface 165 of the upper midsole 147 and the upper surface 166 of the bottom sole 149 when fully loaded under moderate body weight pressure, as indicated in FIG. 9B, or under maximum normal peak landing force during running, as indicated in FIG. 9C, just as the human foot does in FIGS. 42B and 42C. The greater the downward force transmitted through the foot to the shoe, the greater the compression pressure in the cushioning compartment 161 and the greater the resulting tension of the shoe sole sides.

FIG. 9D shows the same shoe sole design when fully loaded and tilted to the natural 20 degree lateral limit, like FIG. 41D. FIG. 9D shows that an added stability benefit of the natural cushioning system for shoe soles is that the effective thickness of the shoe sole is reduced by compression on the side so that the potential destabilizing lever arm represented by the shoe sole thickness is also reduced, so foot and ankle stability is increased. Another benefit of the FIG. 9 design is that the upper midsole shoe surface can move in any horizontal direction, either sideways or front to back in order to absorb shearing forces, that shearing motion is controlled by tension in the sides. Note that the right side of FIGS. 9A–D is modified to provide a natural crease or upward taper 162, which allows complete side compression without binding or bunching between the upper and lower shoe sole layers 147, 148, and 149; the shoe sole crease 162 parallels exactly a similar crease or taper 163 in the human foot.

Another possible variation of joining shoe upper to shoe bottom sole is on the right (lateral) side of FIGS. 9A–D, which makes use of the fact that it is optimal for the tension absorbing shoe sole sides, whether shoe upper or bottom sole, to coincide with the Theoretically Ideal Stability Plane alone the side of the shoe sole beyond that point reached when the shoe is tilted to the foot's natural limit, so that no destabilizing shoe sole lever arm is created when the shoe is tilted fully, as in FIG. 9D. The joint may be moved up slightly so that the fabric side does not come in contact with the ground, or it may be cover with a coating to provide both traction and fabric protection.

It should be noted that the FIG. 9 design provides a structural basis for the shoe sole to conform very easily to the natural shape of the human foot and to parallel easily the natural deformation flattening of the foot during load-bearing motion on the ground. This is true even if the shoe sole is made conventionally with a flat sole, as lone as rigid structures such as heel counters and motion control devices are not used; though not optimal, such a conventional flat shoe made like FIG. 9 would provide the essential features of the new invention resulting in significantly improved cushioning and stability. The FIG. 9 design could also be applied to intermediate-shaped shoe soles that neither conform to the flat ground or the naturally contoured foot. In addition, the FIG. 9 design can be applied to the applicant's other designs, such as those described in his pending U.S. application Ser. No. 07/416,478, filed on Oct. 3. 1989.

In summary, the FIG. 9 design shows a shoe construction for a shoe, including: a shoe sole with a compartment or compartments under the structural elements of the human

foot, including at least the heel; the compartment or compartments contains a pressure-transmitting medium like liquid, gas, or gel; a portion of the upper surface of the shoe sole compartment firmly contacts the lower surface of said compartment during normal load-bearing; and pressure from the load-bearing is transmitted progressively at least in part to the relatively inelastic sides, top and bottom of the shoe sole compartment or compartments, producing tension.

The applicant's FIG. 9 invention can be combined with the FIG. 3 invention, although the combination is not shown; the FIG. 9 invention can be combined with FIGS. 10 and 11 below. Also not shown, but useful combinations, is the applicant's FIGS. 3, 10 and 11 inventions with all of the applicant's deformation sipes inventions, the first of a sequence of applications on various embodiments of that sipes invention is U.S. Ser. No. 07/424,509, filed Oct. 20, 1989, and with his inventions based on other sagittal plane or long axis shoe sole thickness variations described in U.S. application Ser. No. 07/469,313, filed Jan. 24, 1990.

All of the applicant's shoe sole invention mentioned immediately above maintain intact the firm lateral stability of the wearer's foot, that stability as demonstrated when the wearer's foot is unshod and tilted out laterally in inversion to the extreme limit of the normal range of motion of the ankle joint of the foot; in a similar demonstration in a conventional shoe sole, the wearer's foot and ankle are unstable. The sides of the applicant's shoe sole invention extend sufficiently far up the sides of the wearer's foot sole to maintain the lateral stability of the wearer's foot when bare.

In addition, the applicant's invention maintains the natural stability and natural, uninterrupted motion of the foot when bare throughout its normal range of sideways pronation and supination motion occurring during all load-bearing phases of locomotion of the wearer, including when said wearer is standing, walking, jogging and running, even when the foot is tilted to the extreme limit of that normal range, in contrast to unstable and inflexible conventional shoe soles, including the partially contoured existing art described above. The sides of the applicant's shoe sole invention extend sufficiently far up the sides of the wearer's foot sole to maintain the natural stability and uninterrupted motion of the wearer's foot when bare. The exact material density of the shoe sole sides will be determined empirically for individuals and groups using standard biomechanical techniques of gait analysis to determine those combinations that best provide the barefoot stability described above.

For the shoe sole combination inventions list immediately above, the amount of any shoe sole side portions coplanar with the theoretically ideal stability plane is determined by the degree of shoe sole stability desired and the shoe sole weight and bulk required to provide said stability; the amount of said coplanar contoured sides that is provided said shoe sole being sufficient to maintain intact the firm stability of the wearer's foot throughout the range of foot inversion and eversion motion typical of the use for which the shoe is intended and also typical of the kind of wearer—such as normal or as excessive pronator—for which said shoe is intended.

Finally, the shoe sole sides are sufficiently flexible to bend out easily when the shoes are put on the wearer's feet and therefore the shoe soles gently hold the sides of the wearer's foot sole when on, providing the equivalent of custom fit in a mass-produced shoe sole. In general, the applicant's preferred shoe sole embodiments include the structural and material flexibility to deform in parallel to the natural deformation of the wearer's foot sole as if it were bare and

unaffected by any of the abnormal foot biomechanics created by rigid conventional shoe sole.

At the same time, the applicant's preferred shoe sole embodiments are sufficiently firm to provide the wearer's foot with the structural support necessary to maintain normal pronation and supination, as if the wearer's foot were bare; in contrast, the excessive softness of many of the shoe sole materials used in shoe soles in the existing art cause abnormal foot pronation and supination.

FIG. 10 is new with this application and is a combination of the shoe sole structure concepts of FIG. 3 and FIG. 4; it combines the custom fit design with the contoured sides greater than the theoretically ideal stability plane. It would apply as well to the FIG. 7 design with contoured sides less than the theoretically ideal stability plane, but that combination is not shown. It would also apply to the FIG. 8 design, which shows a bottom sole tread design, but that combination is also not shown.

While the FIG. 3 custom fit invention is novel for shoe sole structures as defined by the theoretically ideal stability plane, which specifies constant shoe sole thickness in frontal or transverse plane, the FIG. 3 custom fit invention is also novel for shoe sole structures with sides that exceed the theoretically ideal stability plane: that is, a shoe sole with thickness greater in the sides than underneath the foot. It would also be novel for shoe sole structures with sides that are less than the theoretically ideal stability plane, within the parameters defined in the '714 application. And it would be novel for a shoe sole structure that provides stability like the barefoot, as described in FIGS. 1 and 2 of the '714 application.

In its simplest conceptual form, the applicant's invention is the structure of a conventional shoe sole that has been modified by having its sides bent up so that their inner surface conforms to a shape nearly identical but slightly smaller than the shape of the outer surface of the foot sole of the wearer (instead of the shoe sole sides conforming to the ground by paralleling it, as is conventional); this concept is like that described in FIG. 3 of the applicant's Ser. No. 07/239,667 application. For the applicant's fully contoured design described in FIG. 15 of the '667 application, the entire shoe sole—including both the sides and the portion directly underneath the foot—is bent up to conform to a shape nearly identical but slightly smaller than the contoured shape of the unloaded foot sole of the wearer, rather than the partially flattened load-bearing foot sole shown in FIG. 3.

This theoretical or conceptual bending up must be accomplished in practical manufacturing without any of the puckering distortion or deformation that would necessarily occur if such a conventional shoe sole were actually bent up simultaneously along all of its the sides; consequently, manufacturing techniques that do not require any bending up of shoe sole material, such as injection molding manufacturing of the shoe sole, would be required for optimal results and therefore is preferable.

It is critical to the novelty of this fundamental concept that all layers of the shoe sole are bent up around the foot sole. A small number of both street and athletic shoe soles that are commercially available are naturally contoured to a limited extent in that only their bottom soles, which are about one quarter to one third of the total thickness of the entire shoe sole, are wrapped up around portions of the wearers, foot soles; the midsole and heel lift (or heel) of such shoe soles, constituting over half of the thickness of the entire shoe sole, remains flat, conforming to the ground rather than the wearers' feet. (At the other extreme, some shoes in the

existing art have flat midsoles and bottom soles, but have insoles that conform to the wearer's foot sole.)

Consequently, in existing contoured shoe soles, the total shoe sole thickness of the contoured side portions is much less than the total thickness of the sole portion directly underneath the foot, whereas in the applicant's shoe sole FIG. **10** invention the shoe sole thickness of the contoured side portions are the at least similar to the thickness of the sole portion directly underneath the foot.

This major and conspicuous structural difference between the applicant's underlying concept and the existing shoe sole art is paralleled by a similarly dramatic functional difference between the two: the aforementioned similar thickness of the applicant's shoe sole invention maintains intact the firm lateral stability of the wearer's foot, that stability as demonstrated when the wearer's foot is unshod and tilted out laterally in inversion to the extreme limit of the normal range of motion of the ankle joint of the foot; in a similar demonstration in a conventional shoe sole, the wearer's foot and ankle are unstable. The sides of the applicant's shoe sole invention extend sufficiently far up the sides of the wearer's foot sole to maintain the lateral stability of the wearer's foot when bare.

In addition, the applicant's invention maintains the natural stability and natural, uninterrupted motion of the foot when bare throughout its normal range of sideways pronation and supination motion occurring during all load-bearing phases of locomotion of the wearer, including when said wearer is standing, walking, jogging and running, even when the foot is tilted to the extreme limit of that normal range, in contrast to unstable and inflexible conventional shoe soles, including the partially contoured existing art described above. The sides of the applicant's shoe sole invention extend sufficiently far up the sides of the wearer's foot sole to maintain the natural stability and uninterrupted motion of the wearer's foot when bare. The exact thickness and material density of the shoe sole sides and their specific contour will be determined empirically for individuals and groups using standard biomechanical techniques of gait analysis to determine those combinations that best provide the barefoot stability described above.

For the FIG. **10** shoe sole invention, the amount of any shoe sole side portions coplanar with the theoretically ideal stability plane is determined by the degree of shoe sole stability desired and the shoe sole weight and bulk required to provide said stability; the amount of said coplanar contoured sides that is provided said shoe sole being sufficient to maintain intact the firm stability of the wearer's foot throughout the range of foot inversion and eversion motion typical of the use for which the shoe is intended and also typical of the kind of wearer—such as normal or as excessive pronator—for which said shoe is intended.

Finally, the shoe sole sides are sufficiently flexible to bend out easily when the shoes are put on the wearer's feet and therefore the shoe soles gently hold the sides of the wearer's foot sole when on, providing the equivalent of custom fit in a mass-produced shoe sole. In general, the applicant's preferred shoe sole embodiments include the structural and material flexibility to deform in parallel to the natural deformation of the wearer's foot sole as if it were bare and unaffected by any of the abnormal foot biomechanics created by rigid conventional shoe sole.

At the same time, the applicant's preferred shoe sole embodiments are sufficiently firm to provide the wearer's foot with the structural support necessary to maintain normal pronation and supination, as if the wearer's foot were bare; in contrast, the excessive softness of many of the shoe sole

materials used in shoe soles in the existing art cause abnormal foot pronation and supination.

As mentioned earlier regarding FIG. **1A** and FIG. **3**, the applicant has previously shown heel lift with constant frontal or transverse plane thickness, since it is oriented conventionally in alignment with the frontal or transverse plane and perpendicular to the long axis of the shoe sole. However, the heel wedge (or toe taper or other shoe sole thickness variations in the sagittal plane along the long axis of the shoe sole) can be located at an angle to the conventional alignment in the FIG. **10** design.

For example, the heel wedge can be located perpendicular to the subtalar axis, which is located in the heel area generally about 20 to 25 degrees medially, although a different angle can be used base on individual or group testing; such a orientation may provide better, more natural support to the subtalar joint, through which critical pronation and supination motion occur. The applicant's theoretically ideal stability plane concept would teach that such a heel wedge orientation would require constant shoe sole thickness in a vertical plane perpendicular to the chosen subtalar joint axis, instead of the frontal plane.

Besides providing a better fit, the intentional undersizing of the flexible shoe sole sides allows for simplified design of shoe sole lasts, since the shoe last needs only to be approximate to provide a virtual custom fit, due to the flexible sides. As a result, the undersized flexible shoe sole sides allow the applicant's FIG. **10** shoe sole invention based on the theoretically ideal stability plane to be manufactured in relatively standard sizes in the same manner as are shoe uppers, since the flexible shoe sole sides can be built on standard shoe lasts, even though conceptually those sides conform to the specific shape of the individual wearer's foot sole, because the flexible sides bend to so conform when on the wearer's foot sole.

FIG. **10** shows the shoe sole structure when not on the foot of the wearer; the dashed line **29** indicates the position of the shoe last, which is assumed to be a reasonably accurate approximation of the shape of the outer surface of the wearer's foot sole, which determines the shape of the theoretically ideal stability plane **51**. Thus, the dashed lines **29** and **51** show what the positions of the inner surface **30** and outer surface **31** of the shoe sole would be when the shoe is put on the foot of the wearer.

The FIG. **10** invention provides a way make the inner surface **30** of the contoured shoe sole, especially its sides, conform very closely to the outer surface **29** of the foot sole of a wearer. It thus makes much more practical the applicant's earlier underlying naturally contoured designs shown in FIGS. **4** and **5**. The shoe sole structures shown in FIGS. **4** and **5**, then, are what the FIG. **10** shoe sole structure would be when on the wearer's load-bearing foot, where the inner surface **30** of the shoe upper is bent out to virtually coincide with the outer surface of the foot sole of the wearer **29** (the figures in this and prior applications show one line to emphasize the conceptual coincidence of what in fact are two lines; in real world embodiments, some divergence of the surface, especially under load and during locomotion would be unavoidable).

The sides of the shoe sole structure described under FIG. **10** can also be used to form a slightly less optimal structure: a conventional shoe sole that has been modified by having its sides bent up so that their inner surface conforms to shape nearly identical but slightly larger than the shape of the outer surface of the foot sole of the wearer, instead of the shoe sole sides being flat on the ground, as is conventional. Clearly, the closer the sides are to the shape of the wearer's foot sole,

the better as a general rule, but any side position between flat on the ground and conforming like FIG. **10** to a shape slightly smaller than the wearer's shape is both possible and more effective than conventional flat shoe sole sides. And in some cases, such as for diabetic patients, it may be optimal to have relatively loose shoe sole sides providing no conforming pressure of the shoe sole on the tender foot sole; in such cases, the shape of the flexible shoe uppers, which can even be made with very elastic materials such as lycra and spandex, can provide the capability for the shoe, including the shoe sole, to conform to the shape of the foot.

As discussed earlier by the applicant, the critical functional feature of a shoe sole is that it deforms under a weight-bearing load to conform to the foot sole just as the foot sole deforms to conform to the ground under a weight-bearing load. So, even though the foot sole and the shoe sole may start in different locations—the shoe sole sides can even be conventionally flat on the ground—the critical functional feature of both is that they both conform under load to parallel the shape of the ground, which conventional shoes do not, except when exactly upright. Consequently, the applicant's shoe sole invention, stated most broadly, includes any shoe sole—whether conforming to the wearer's foot sole or to the ground or some intermediate position, including a shape much smaller than the wearer's foot sole—that deforms to conform to a shape at least similar to the theoretically ideal stability plane, which by definition itself deforms in parallel with the deformation of the wearer's foot sole under weight-bearing load.

Of course, it is optimal in terms of preserving natural foot biomechanics, which is the primary goal of the applicant, for the shoe sole to conform to the foot sole when on the foot, not just when under a weight-bearing load. And, in any case, all of the essential structural support and propulsion elements previously identified by the applicant earlier in discussing FIG. **3** must be supported by the foot sole.

To the extent the shoe sole sides are easily flexible, as has already been specified as desirable, the position of the shoe sole sides before the wearer puts on the shoe is less important, since the sides will easily conform to the shape of the wearer's foot when the shoe is put on that foot. In view of that, even shoe sole sides that conform to a shape more than slightly smaller than the shape of the outer surface of the wearer's foot sole would function in accordance with the applicant's general invention, since the flexible sides could bend out easily a considerable relative distance and still conform to the wearer's foot sole when on the wearer's foot.

FIG. **11** is new with this application and is a combination of the shoe sole structure concepts of FIG. **3** and FIG. **6**; it combines the custom fit design with the contoured sides having material density variations that produce an effect similar to variations in shoe sole thickness shown in FIGS. **4**, **5**, and **7**; only the midsole is shown. The density variation pattern shown in FIG. **2** can be combined with the type shown in FIG. **11**. The density pattern can be constant in all cross sections taken along the long long axis of the shoe sole or the pattern can vary.

The applicant's FIG. **11** shoe sole invention maintains intact the firm lateral stability of the wearer's foot, that stability as demonstrated when the wearer's foot is unshod and tilted out laterally in inversion to the extreme limit of the normal range of motion of the ankle joint of the foot; in a similar demonstration in a conventional shoe sole, the wearer's foot and ankle are unstable. The sides of the applicant's shoe sole invention extend sufficiently far up the sides of the wearer's foot sole to maintain the lateral stability of the wearer's foot when bare.

In addition, the applicant's invention maintains the natural stability and natural, uninterrupted motion of the foot when bare throughout its normal range of sideways pronation and supination motion occurring during all load-bearing phases of locomotion of the wearer, including when said wearer is standing, walking, jogging and running, even when the foot is tilted to the extreme limit of that normal range, in contrast to unstable and inflexible conventional shoe soles, including the partially contoured existing art described above. The sides of the applicant's shoe sole invention extend sufficiently far up the sides of the wearer's foot sole to maintain the natural stability and uninterrupted motion of the wearer's foot when bare. The exact material density of the shoe sole sides will be determined empirically for individuals and groups using standard biomechanical techniques of gait analysis to determine those combinations that best provide the barefoot stability described above.

For the FIG. **11** shoe sole invention, the amount of any shoe sole side portions coplanar with the theoretically ideal stability plane is determined by the degree of shoe sole stability desired and the shoe sole weight and bulk required to provide said stability; the amount of said coplanar contoured sides that is provided said shoe sole being sufficient to maintain intact the firm stability of the wearer's foot throughout the range of foot inversion and eversion motion typical of the use for which the shoe is intended and also typical of the kind of wearer—such as normal or as excessive pronator—for which said shoe is intended.

Finally, the shoe sole sides are sufficiently flexible to bend out easily when the shoes are put on the wearer's feet and therefore the shoe soles gently hold the sides of the wearer's foot sole when on, providing the equivalent of custom fit in a mass-produced shoe sole. In general, the applicant's preferred shoe sole embodiments include the structural and material flexibility to deform in parallel to the natural deformation of the wearer's foot sole as if it were bare and unaffected by any of the abnormal foot biomechanics created by rigid conventional shoe sole.

At the same time, the applicant's preferred shoe sole embodiments are sufficiently firm to provide the wearer's foot with the structural support necessary to maintain normal pronation and supination, as if the wearer's foot were bare; in contrast, the excessive softness of many of the shoe sole materials used in shoe soles in the existing art cause abnormal foot pronation and supination.

As mentioned earlier regarding FIG. **1A** and FIG. **3**, the applicant has previously shown heel lift with constant frontal or transverse plane thickness, since it is oriented conventionally in alignment with the frontal or transverse plane and perpendicular to the long axis of the shoe sole. However, the heel wedge (or toe taper or other shoe sole thickness variations in the sagittal plane along the long axis of the shoe sole) can be located at an angle to the conventional alignment in the Fiwn q0 design.

For example, the heel wedge can be located perpendicular to the subtalar axis, which is located in the heel area generally about 20 to 25 degrees medially, although a different angle can be used base on individual or group testing; such a orientation may provide better, more natural support to the subtalar joint, through which critical pronation and supination motion occur. The applicant's theoretically ideal stability plane concept would teach that such a heel wedge orientation would require constant shoe sole thickness in a vertical plane perpendicular to the chosen subtalar joint axis, instead of the frontal plane.

Besides providing a better fit, the intentional undersizing of the flexible shoe sole sides allows for simplified design of

shoe sole lasts, since the shoe last needs only to be approximate to provide a virtual custom fit, due to the flexible sides. As a result, the undersized flexible shoe sole sides allow the applicant's FIG. **10** shoe sole invention based on the theoretically ideal stability plane to be manufactured in relatively standard sizes in the same manner as are shoe uppers, since the flexible shoe sole sides can be built on standard shoe lasts, even though conceptually those sides conform to the specific shape of the individual wearer's foot sole, because the flexible sides bend to so conform when on the wearer's foot sole.

Besides providing a better fit, the intentional undersizing of the flexible shoe sole sides allows for simplified design of shoe sole lasts, since they can be designed according to the simple geometric methodology described in the textual specification of FIG. **27**, U.S. application Ser. No. 07/239, 667 (filed 02 Sep. 1988). That geometric approximation of the true actual contour of the human is close enough to provide a virtual custom fit, when compensated for by the flexible undersizing from standard shoe lasts described above.

A flexible undersized version of the fully contoured design described in FIG. **11** can also be provided by a similar geometric approximation. As a result, the undersized flexible shoe sole sides allow the applicant's shoe sole inventions based on the theoretically ideal stability plane to be manufactured in relatively standard sizes in the same manner as are shoe uppers, since the flexible shoe sole sides can be built on standard shoe lasts, even though conceptually those sides conform closely to the specific shape of the individual wearer's foot sole, because the flexible sides bend to conform when on the wearer's foot sole.

FIG. **11** shows the shoe sole structure when not on the foot of the wearer; the dashed line **29** indicates the position of the shoe last, which is assumed to be a reasonably accurate approximation of the shape of the outer surface of the wearer's foot sole, which determines the shape of the theoretically ideal stability plane **51**. Thus, the dashed lines **29** and **51** show what the positions of the inner surface **30** and outer surface **31** of the shoe sole would be when the shoe is put on the foot of the wearer.

The FIG. **11** invention provides a way make the inner surface **30** of the contoured shog sole, especially its sides, conform very closely to the outer surface **29** of the foot sole of a wearer. It thus makes much more practical the applicant's earlier underlying naturally contoured designs shown in FIGS. **1A–C** and FIG. **6**. The shoe sole structure shown in FIG. **61**, then, is what the FIG. **11** shoe sole structure would be when on the wearer's foot, where the inner surface **30** of the shoe upper is bent out to virtually coincide with the outer surface of the foot sole of the wearer **29** (the figures in this and prior applications show one line to emphasize the conceptual coincidence of what in fact are two lines; in real world embodiments, some divergence of the surface, especially under load and during locomotion would be unavoidable).* The sides of the shoe sole structure described under FIG. **11** can also be used to form a slightly less optimal structure: a conventional shoe sole that has been modified by having its sides bent up so that their inner surface conforms to shape nearly identical but slightly larger than the shape of the outer surface of the foot sole of the wearer, instead of the shoe sole sides being flat on the ground, as is conventional. Clearly, the closer the sides are to the shape of the wearer's foot sole, the better as a general rule, but any side position between flat on the ground and conforming like FIG. **11** to a shape slightly smaller than the wearer's shape is both possible and more effective than conventional flat shoe sole

sides. And in some cases, such as for diabetic patients, it may be optimal to have relatively loose shoe sole sides providing no conforming pressure of the shoe sole on the tender foot sole; in such cases, the shape of the flexible shoe uppers, which can even be made with very elastic materials such as lycra and spandex, can provide the capability for the shoe, including the shoe sole, to conform to the shape of the foot.

As discussed earlier by the applicant, the critical functional feature of a shoe sole is that it deforms under a weight-bearing load to conform to the foot sole just as the foot sole deforms to conform to the ground under a weight-bearing load. So, even though the foot sole and the shoe sole may start in different locations—the shoe sole sides can even be conventionally flat on the ground—the critical functional feature of both is that they b th conform under load to parallel the shape of the ground, which conventional shoes do not, except when exactly upright. Consequently, the applicant's shoe sole invention, stated most broadly, includes any shoe sole—whether conforming to the wearer's foot sole or to the ground or some intermediate position, including a shape much smaller than the wearer's foot sole—that deforms to conform to the theoretically ideal stability plane, which by definition itself deforms in parallel with the deformation of the wearer's foot sole under weight-bearing load.

Of course, it is optimal in terms of preserving natural foot biomechanics, which is the primary goal of the applicant, for the shoe sole to conform to the foot sole when on the foot, not just when under a weight-bearing load. And, in any case, all of the essential structural support and propulsion elements previously identified by the applicant earlier in discussing FIG. **3** must be supported by the foot sole.

To the extent the shoe sole sides are easily flexible, as has already been specified as desirable, the position of the shoe sole sides before the wearer puts on the shoe is less important, since the sides will easily conform to the shape of the wearer's foot when the shoe is put on that foot. In view of that, even shoe sole sides that conform to a shape more than slightly smaller than the shape of the outer surface of the wearer's foot sole would function in accordance with the applicant's general invention, since the flexible sides could bend out easily a considerable relative distance and still conform to the wearer's foot sole when on the wearer's foot.

The applicant's shoe sole inventions described in FIGS. **4**, **10** and **11** all attempt to provide structural compensation for actual structural changes in the feet of wearers that have occurred from a lifetime of use of existing shoes, which have a major flaw that has been identified and described earlier by the applicant. As a result, the biomechanical motion of even the wearer's barefeet have been degraded from what they would be if the wearer's feet had not been structurally changed. Consequently, the ultimate design goal of the applicant's inventions is to provide un-degraded barefoot motion. That means to provide wearers with shoe soles that compensate for their flawed barefoot structure to an extent sufficient to provide foot and ankle motion equivalent to that of their barefeet if never shod and therefore not flawed. Determining the biomechanical characteristics of such un-flawed barefeet will be difficult, either on an individual or group basis. The difficulty for many groups of wearers will be in finding un-flawed, never-shod barefoot from similar genetic groups, assuming significant genetic differences exist, as seems at least possible if not probable.

The ultimate goal of the applicant's invention is to provide shoe sole structures that maintain the natural stability and natural, uninterrupted motion of the foot when bare throughout its normal range of sideways pronation and

supination motion occurring during all load-bearing phases
of locomotion of a wearer who has never been shod in
conventional shoes, including when said wearer is standing,
walking, jogging and running, even when the foot is tilted to
the extreme limit of that normal range, in contrast to
unstable and inflexible conventional shoe soles.

FIG. **12** [1] shows in a real illustration a foot **27** in
position for a new biomechanical test that is the basis for the
discovery that ankle sprains are in fact unnatural for the bare
foot. The test simulates a lateral ankle sprain, where the foot
27—on the around **43**—rolls or tilts to the outside, to the
extreme end of its normal range of motion, which is usually
about 20 degrees at the heel **29**, as shown in a rear view of
a bare (right) heel in FIG. **12**. Lateral (inversion) sprains are
the most common ankle sprains, accounting for about three-
fourths of all.

The especially novel aspect of the testing approach is to
perform the ankle spraining simulation while standing sta-
tionary. The absence of forward motion is the key to the
dramatic success of the test because otherwise it is impos-
sible to recreate for testing purposes the actual foot and
ankle motion that occurs during a lateral ankle sprain, and
simultaneously to do it in a controlled manner, while at
normal running speed or even jogging slowly, or walking.
Without the critical control achieved by slowing forward
motion all the way down to zero, any test subject would end
up with a sprained ankle.

That is because actual running in the real world is
dynamic and involves a repetitive force maximum of three
times one's full body weight for each footstep, with sudden
peaks up to roughly five or six times for quick stops,
missteps, and direction changes, as might be experienced
when spraining an ankle. In contrast, in the static simulation
test, the forces are tightly controlled and moderate, ranging
from no force at all up to whatever maximum amount that
is comfortable.

The Stationary Sprain Simulation Test (SSST) consists
simply of standing stationary with one foot bare and the
other shod with any shoe. Each foot alternately is carefully
tilted to the outside up to the extreme end of its range of
motion, simulating a lateral ankle sprain.

The Stationary Sprain Simulation Test clearly identifies
what can be no less than a fundamental flaw in existing shoe
design. It demonstrates conclusively that nature's biome-
chanical system, the bare foot, is far superior in stability to
man's artificial shoe design. Unfortunately, it also demon-
strates that the shoe's severe instability overpowers the
natural stability of the human foot and synthetically creates
a combined biomechanical system that is artificially
unstable. The shoe is the weak link.

The test shows that the bare foot is inherently stable at the
approximate 20 degree end of normal joint range because of
the wide, steady foundation the bare heel **29** provides the
ankle joint, as seen in FIG. **12**. In fact, the area of physical
contact of the bare heel **29** with the around **43** is not much
less when tilted all the way out to 20 degrees as when upright
at 0 degrees.

The new Stationary Sprain Simulation Test provides a
natural yardstick, totally missing until now, to determine
whether any given shoe allows the foot within it to function
naturally. If a shoe cannot pass this simple litmus test, it is
positive proof that a particular shoe is interfering with
natural foot and ankle biomechanics. The only question is
the exact extent of the interference beyond that demon-
strated by the new test.

Conversely, the applicant's designs are the only designs
with shoe soles thick enough to provide cushioning (thin-

soled and heel-less moccasins do pass the test, but do not
provide cushioning and only moderate protection) that will
provide naturally stable performance, like the bare foot, in
the Stationary Sprain Simulation Test.

FIG. **13** [2] shows that, in complete contrast the foot
equipped with a conventional running shoe, designated
generally by the reference numeral **20** and having an upper
21, though initially very stable while resting completely flat
on the ground, becomes immediately unstable when the shoe
sole **22** is tilted to the outside. The tilting motion lifts from
contact with the ground all of the shoe sole **22** except the
artificially sharp edge of the bottom outside corner. The shoe
sole instability increases the farther the foot is rolled later-
ally. Eventually, the instability induced by the shoe itself is
so great that the normal load-bearing pressure of full body
weight would actively force an ankle sprain if not controlled.
The abnormal tilting motion of the shoe does not stop at the
barefoot's natural 20 degree limit, as you can see from the
45 degree tilt of the shoe heel in FIG. **13**.

That continued outward rotation of the shoe past **20**
degrees causes the foot to slip within the shoe, shifting its
position within the shoe to the outside edge, further increas-
ing the shoe's structural instability. The slipping of the foot
within the shoe is caused by the natural tendency of the foot
to slide down the typically flat surface of the tilted shoe sole;
the more the tilt, the stronger the tendency. The heel is
shown in FIG. **13** because of its primary importance in
sprains due to its direct physical connection to the ankle
ligaments that are torn in an ankle sprain and also because
of the heel's predominant role within the foot in bearing
body weight.

It is easy to see in the two figures how totally different the
physical shape of the natural bare foot is compared to the
shape of the artificial shoe sole. It is strikingly odd that the
two objects, which apparently both have the same biome-
chanical function, have completely different physical
shapes. Moreover, the shoe sole clearly does not deform the
same way the human foot sole does, primarily as a conse-
quence of its dissimilar shape.

FIG. **14**A [3] illustrates that the underlying problem with
existing shoe designs is fairly easy to understand by looking
closely at the principal forces acting on the physical struc-
ture of the shoe sole. When the shoe is tilted outwardly, the
weight of the body held in the shoe upper **21** shifts auto-
matically to the outside edge of the shoe sole **22**. But, strictly
due to its unnatural shape, the tilted shoe sole **22** provides
absolutely no supporting physical structure directly under-
neath the shifted body weight where it is critically needed to
support that weight. An essential part of the supporting
foundation is missing. The only actual structural support
comes from the sharp corner edge **23** of the shoe sole **22**,
which unfortunately is not directly under the force of the
body weight after the shoe is tilted. Instead, the corner edge
23 is offset well to the inside.

As a result of that unnatural misalignment, a lever arm
23a is set up through the shoe sole **22** between two inter-
acting forces (called a force couple): the force of gravity on
the body (usually known as body weight **133**) applied at the
point **24** in the upper **21** and the reaction force **134** of the
ground, equal to and opposite to body weight when the shoe
is upright. The force couple creates a force moment, com-
monly called torque, that forces the shoe **20** to rotate to the
outside around the sharp corner edge **23** of the bottom sole
22, which serves as a stationary pivoting point **23** or center
of rotation.

Unbalanced by the unnatural geometry of the shoe sole
when tilted, the opposing two forces produce torque, causing

the shoe 20 to tilt even more. As the shoe 20 tilts further, the torque forcing the rotation becomes even more powerful, so the tilting process becomes a self-reenforcing cycle. The more the shoe tilts, the more destabilizing torque is produced to further increase the tilt.

The problem may be easier to understand by looking at the diagram of the force components of body weight shown in FIG. 14A.

When the shoe sole 22 is tilted out 45 degrees, as shown, only half of the downward force of body weight 133 is physically supported by the shoe sole 22; the supported force component 135 is 71% of full body weight 133. The other half of the body weight at the 45 degree tilt is unsupported physically by any shoe sole structure; the unsupported component is also 71% of full body weight 133. It therefore produces strong destabilizing outward tilting rotation, which is resisted by nothing structural except the lateral ligaments of the ankle.

FIG. 14B show that the full force of body weight 133 is split at 45 degrees of tilt into two equal components: supported 135 and unsupported 136, each equal to 0.707 of full body weight 133. The two vertical components 137 and 138 of body weight 133 are both equal to 0.50 of full body weight. The ground reaction force 134 is equal to the vertical component 137 of the supported component 135.

FIG. 15 [4] show a summary of the force components at shoe sole tilts of 0, 45 and 90 degrees. FIG. 15, which uses the same reference numerals as in FIG. 14, shows that, as the outward rotation continues to 90 degrees, and the foot slips within the shoe while ligaments stretch and/or break, the destabilizing unsupported force component 136 continues to grow. When the shoe sole has tilted all the way out to 90 degrees (which unfortunately does happen in the real world), the sole 22 is providing no structural support and there is no supported force component 135 of the full body weight 133. The around reaction force at the pivoting point 23 is zero, since it would move to the upper edge 24 of the shoe sole.

At that point of 90 decree tilt, all of the full body weight 133 is directed into the unresisted and unsupported force component 136, which is destabilizing the shoe sole very powerfully. In other words, the full weight of the body is physically unsupported and therefore powering the outward rotation of the shoe sole that produces an ankle sprain. Insidiously, the farther ankle ligaments are stretched, the greater the force on them.

In stark contrast, untilted at 0 degrees, when the shoe sole is upright, resting flat on the ground, all of the force of body weight 133 is Physically supported directly by the shoe sole and therefore exactly equals the supported force component 135, as also shown in FIG. 15. In the untilted position, there is no destabilizing unsupported force component 136.

FIG. 16 [5] illustrates that the extremely rigid heel counter 141 typical of existing athletic shoes, together with the motion control device 142 that are often used to strongly reinforce those heel counters (and sometimes also the sides of the mid- and forefoot), are ironically counterproductive. Though they are intended to increase stability, in fact they decrease it. FIG. 16 shows that when the shoe 20 is tilted out, the foot is shifted within the upper 21 naturally against the rigid structure of the typical motion control device 142, instead of only the outside edge of the shoe sole 22 itself. The motion control support 142 increases by almost twice the effective lever arm 132 (compared to 23a) between the force couple of body weight and the ground reaction force at the pivot point 23. It doubles the destabilizing torque and also increases the effective angle of tilt so that the destabilizing force component 136 becomes greater compared to

the supported component 135, also increasing the destabilizing torque. To the extent the foot shifts further to the outside, the problem becomes worse. Only by removing the heel counter 141 and the motion control devices 142 can the extension of the destabilizing lever arm be avoided. Such an approach would primarily rely on the applicant's contoured shoe sole to "cup" the foot (especially the heel), and to a much lesser extent the non-rigid fabric or other flexible material of the upper 21, to position the foot, including the heel, on the shoe. Essentially, the naturally contoured sides of the applicant's shoe sole replace the counter-productive existing heel counters and motion control devices, including those which extend around virtually all of the edge of the foot.

FIG. 17 [6] shows that the same kind of torsional problem, though to a much more moderate extent, can be produced in the applicant's naturally contoured design of the applicant's earlier filed applications. There, the concept of a theoretically-ideal stability plane was developed in terms of a sole 28 having a lower surface 31 and an upper surface 30 which are spaced apart by a predetermined distance which remains constant throughout the sagittal frontal planes. The outer surface 27 of the foot is in contact with the upper surface 30 of the sole 28. Though it might seem desirable to extend the inner surface 30 of the shoe sole 28 up around the sides of the foot 27 to further support it (especially in creating anthropomorphic designs), FIG. 17 indicates that only that portion of the inner shoe sole 28 that is directly supported structurally underneath by the rest of the shoe sole is effective in providing natural support and stability. Any point on the upper surface 30 of the shoe sole 28 that is not supported directly by the constant shoe sole thickness (as measured by a perpendicular to a tangent at that point and shown in the shaded area 143) will tend to produce a moderate destabilizing torque. To avoid creating a destabilizing lever arm 132, only the supported contour sides and non-rigid fabric or other material can be used to position the foot on the shoe sole 28.

FIG. 18 [7] illustrates an approach to minimize structurally the destabilizing lever arm 32 and therefore the potential torque problem. After the last point where the constant shoe sole thickness (s) is maintained, the finishing edge of the shoe sole 28 should be tapered gradually inward from both the top surface 30 and the bottom surface 31, in order to provide matching rounded or semi-rounded edges. In that way, the upper surface 30 does not provide an unsupported portion that creates a destabilizing torque and the bottom surface 31 does not provide an unnatural pivoting edge. The gap 144 between shoe sole 28 and foot sole 29 at the edge of the shoe sole can be "caulked" with exceptionally soft sole material as indicated in FIG. 18 that, in the aggregate (i.e, all the way around the edge of the shoe sole), will help position the foot in the shoe sole. However, at any point of pressure when the shoe tilts, it will deform easily so as not to form an unnatural lever causing a destabilizing torque.

FIG. 19 [11] illustrates a fully contoured design, but abbreviated along the sides to only essential structural stability and propulsion shoe sole elements as shown in FIG. 21 of U.S. patent application Ser. No. 07/239,667 (filed 02 Sep. 1988) combined with the freely articulating structural elements underneath the foot as shown in FIG. 28 of the same patent application. The unifying concept is that, on both the sides and underneath the main load-bearing portions of the shoe sole, only the important structural (i.e. bone) elements of the foot should be supported by the shoe sole, if the natural flexibility of the foot is to be paralleled accurately in shoe sole flexibility, so that the shoe sole does

not interfere with the foot's natural motion. In a sense, the shoe sole should be composed of the same main structural elements as the foot and they should articulate with each other lust as do the main joints of the foot.

FIG. 19E shows the horizontal plane bottom view of the right foot corresponding to the fully contoured design previously described, but abbreviated alone the sides to only essential structural support and propulsion elements. Shoe sole material density can be increased in the unabbreviated essential elements to compensate for increased pressure loading there. The essential structural support elements are the base and lateral tuberosity of the calcaneus 95, the heads of the metatarsals 96, and the base of the fifth metatarsal 97 (and the adjoining cuboid in some individuals). They must be supported both underneath and to the outside edge of the foot for stability. The essential propulsion element is the head of the first distal phalange 98. FIG. 19 shows that the naturally contoured stability sides need not be used except in the identified essential areas. Weight savings and flexibility improvements can be made by omitting the non-essential stability sides.

The design of the portion of the shoe sole directly underneath the foot shown in FIG. 19 allows for unobstructed natural inversion/eversion motion of the calcaneus by providing maximum shoe sole flexibility Particularly between the base of the calcaneus 125 (heel) and the metatarsal heads 126 (forefoot) along an axis 120. An unnatural torsion occurs about that axis if flexibility is insufficient so that a conventional shoe sole interferes with the inversion/eversion motion by restraining it. The object of the design is to allow the relatively more mobile (in inversion and eversion) calcaneus to articulate freely and independently from the relatively more fixed forefoot instead of the fixed or fused structure or lack of stable structure between the two in conventional designs. In a sense, freely articulating joints are created in the shoe sole that parallel those of the foot. The design is to remove nearly all of the shoe sole material between the heel and the forefoot, except under one of the previously described essential structural support elements, the base of the fifth metatarsal 97. An optional support for the main longitudinal arch 121 may also be retained for runners with substantial foot pronation, although would not be necessary for many runners.

The forefoot can be subdivided (not shown) into its component essential structural support and propulsion elements, the individual heads of the metatarsal and the heads of the distal phalanges, so that each major articulating joint set of the foot is paralleled by a freely articulating shoe sole support propulsion element, an anthropomorphic design; various aggregations of the subdivision are also possible.

The design in FIG. 19 features an enlarged structural support at the base of the fifth metatarsal in order to include the cuboid, which can also come into contact with the around under arch compression in some individuals. In addition, the design can provide general side support in the heel area, as in FIG. 19E or alternatively can carefully orient the stability sides in the heel area to the exact positions of the lateral calcaneal tuberosity 108 and the main base of the calcaneus 109, as in FIG. 19E' (showing heel area only of the right foot). FIGS. 19A–D show frontal plane cross sections of the left shoe and FIG. 19E shows a bottom view of the right foot, with flexibility axes 120, 122, 111, 112 and 113 indicated. FIG. 19F shows a sagittal plane cross section showing the structural elements joined by very thin and relatively soft upper midsole layer. FIGS. 19G and 19H show similar cross sections with slightly different designs featuring durable fabric only (slip-lasted shoe), or a struc-

turally sound arch design, respectively. FIG. 19I shows a side medial view of the shoe sole.

FIG. 19J shows a simple interim or low cost construction for the articulating shoe sole support element 95 for the heel (showing the heel area only of the right foot); while it is most critical and effective for the heel support element 95, it can also be used with the other elements, such as the base of the fifth metatarsal 97 and the long arch 121. The heel sole element 95 shown can be a single flexible layer or a lamination of layers. When cut from a flat sheet or molded in the general pattern shown, the outer edges can be easily bent to follow the contours of the foot, particularly the sides. The shape shown allows a flat or slightly contoured heel element 95 to be attached to a highly contoured shoe upper or very thin upper sole layer like that shown in FIG. 19F. Thus, a very simple construction technique can yield a highly sophisticated shoe sole design. The size of the center section 119 can be small to conform to a fully or nearly fully contoured design or larger to conform to a contoured sides design, where there is a large flattened sole area under the heel. The flexibility is provided by the removed diagonal sections, the exact proportion of size and shape can vary.

FIG. 20 [12] illustrates an expanded explanation of the correct approach for measuring shoe sole thickness according to the naturally contoured design, as described previously in FIGS. 23 and 24 of U.S. patent application Ser. No. 07/239,667 (filed 02 Sep. 1988). The tangent described in those figures would be parallel to the ground when the shoe sole is tilted out sideways, so that measuring shoe sole thickness alone the perpendicular will provide the least distance between the point on the upper shoe sole surface closest to the ground and the closest point to it on the lower surface of the shoe sole (assuming no load deformation).

FIG. 21 [13] shows a non-optimal but interim or low cost approach to shoe sole construction, whereby the midsole and heel lift 127 are Produced conventionally, or nearly so (at least leaving the midsole bottom surface flat, though the sides can be contoured), while the bottom or outer sole 128 includes most or all of the special contours of the new design. Not only would that completely or mostly limit the special contours to the bottom sole, which would be molded specially, it would also ease assembly, since two flat surfaces of the bottom of the midsole and the top of the bottom sole could be mated together with less difficulty than two contoured surfaces, as would be the case otherwise. The advantage of this approach is seen in the naturally contoured design example illustrated in FIG. 21A, which shows some contours on the relatively softer midsole sides, which are subject to less wear but benefit from greater traction for stability and ease of deformation, while the relatively harder contoured bottom sole provides good wear for the load-bearing areas. FIG. 21B shows in a quadrant side design the concept applied to conventional street shoe heels, which are usually separated from the forefoot by a hollow instep area under the main longitudinal arch. FIG. 21C shows in frontal plane cross section the concept applied to the quadrant sided or single plane design and indicating in FIG. 21D in the shaded area 129 of the bottom sole that portion which should be honeycombed (axis on the horizontal plane) to reduce the density of the relatively hard outer sole to that of the midsole material to provide for relatively uniform shoe density. FIG. 21E shows in bottom view the outline of a bottom sole 128 made from flat material which can be conformed topologically to a contoured midsole of either the one or two plane designs by limiting the side areas to be mated to the essential support areas discussed in FIG. 21 of the '667 application; by that method, the contoured midsole and flat bottom sole

surfaces can be made to join satisfactorily by coinciding closely, which would be topologically impossible if all of the side areas were retained on the bottom sole.

FIGS. **22A–22C** [14], frontal plane cross sections, show an enhancement to the previously described embodiments of the shoe sole side stability quadrant invention of the '349 Patent. As stated earlier, one major purpose of that design is to allow the shoe sole to pivot easily from side to side with the foot **90**, thereby following the foot's natural inversion and eversion motion; in conventional designs shown in FIG. **22a,** such foot motion is forced to occur within the shoe upper **21**, which resists the motion. The enhancement is to position exactly and stabilize the foot, especially the heel, relative to the preferred embodiment of the shoe sole; doing so facilitates the shoe sole's responsiveness in following the foot's natural motion. Correct positioning is essential to the invention, especially when the very narrow or "hard tissue" definition of heel width is used. Incorrect or shifting relative position will reduce the inherent efficiency and stability of the side quadrant design, by reducing the effective thickness of the quadrant side **26** to less than that of the shoe sole **28***b*. As shown in FIG. **22B** and **22C**, naturally contoured inner stability sides **131** hold the pivoting edge **31** of the load-bearing foot sole in the correct position for direct contact with the flat upper surface of the conventional shoe sole **22**, so that the shoe sole thickness (s) is maintained at a constant thickness (s) in the stability quadrant sides **26** when the shoe is everted or inverted, following the theoretically ideal stability plane **51**.

The form of the enhancement is inner shoe sole stability sides **131** that follow the natural contour of the sides **91** of the heel of the foot **90**, thereby cupping the heel of the foot. The inner stability sides **131** can be located directly on the top surface of the shoe sole and heel contour, or directly under the shoe insole (or integral to it), or somewhere in between. The inner stability sides are similar in structure to heel cups integrated in insoles currently in common use, but differ because of its material density, which can be relatively firm like the typical mid-sole, not soft like the insole. The difference is that because of their higher relative density, preferably like that of the uppermost midsole, the inner stability sides function as part of the shoe sole, which provides structural support to the foot, not just gentle cushioning and abrasion protection of a shoe insole. In the broadest sense, though, insoles should be considered structurally and functionally as part of the shoe'sole, as should any shoe material between foot and ground, like the bottom of the shoe upper in a slip-lasted shoe or the board in a board-lasted shoe.

The inner stability side enhancement is particularly useful in converting existing conventional shoe sole design embodiments **22**, as constructed within prior art, to an effective embodiment of the side stability quadrant **26** invention. This feature is important in constructing prototypes and initial production of the invention, as well as an ongoing method of low cost production, since such production would be very close to existing art.

The inner stability sides enhancement is most essential in cupping the sides and back of the heel of the foot and therefore is essential on the upper edge of the heel of the shoe sole **27**, but may also be extended around all or any portion of the remaining shoe sole upper edge. The size of the inner stability sides should, however, taper down in proportion to any reduction in shoe sole thickness in the sagittal plane.

FIGS. **23A–23C** [15], frontal plane cross sections, illustrate the same inner shoe sole stability sides enhancement as it applies to the previously described embodiments of the naturally contoured sides '667 application design. The enhancement positions and stabilizes the foot relative to the shoe sole, and maintains the constant shoe sole thickness (s) of the naturally contoured sides **28***a* design, as shown in FIGS. **23B** and **23C**; FIG. **23A** shows a conventional design. The inner shoe sole stability sides **131** conform to the natural contour of the foot sides **29**, which determine the theoretically ideal stability plane **51** for the shoe sole thickness (s). The other features of the enhancement as it applies to the naturally contoured shoe sole sides embodiment **28** are the same as described previously under FIGS. **22A–22C** for the side stability quadrant embodiment. It is clear from comparing FIGS. **23C** and **22C** that the two different approaches, that with quadrant sides and that with naturally contoured sides, can yield some similar resulting shoe sole embodiments through the use of inner stability sides **131**. In essence, both approaches provide a low cost or interim method of adapting existing conventional "flat sheet" shoe manufacturing to the naturally contoured design described in previous figures.

FIGS. **24**, **25**, and **26** [1–3] show frontal plane cross sectional views of a shoe sole according to the applicant's prior inventions based on the theoretically ideal stability plane, taken at about the ankle joint to show the heel section of the shoe. FIGS. **4**, **5**, **8**, and **27–32** show the same view of the applicant's enhancement of that invention. The reference numerals are like those used in the prior pending applications of the applicant mentioned above and which are incorporated by reference for the sake of completeness of disclosure, if necessary. In the figures, a foot **27** is positioned in a naturally contoured shoe having an upper **21** and a sole **28**. The shoe sole normally contacts the ground **43** at about the lower central heel portion thereof, as shown in FIG. **4**. The concept of the theoretically ideal stability plane, as developed in the prior applications as noted, defines the plane **51** in terms of a locus of points determined by the thickness(es) of the sole.

FIG. **24** [1] shows, in a rear cross sectional view, the application of the prior invention showing the inner surface of the shoe sole conforming to the natural contour of the foot and the thickness of the shoe sole remaining constant in the frontal plane, so that the outer surface coincides with the theoretically ideal stability plane.

FIG. **25** [2] shows a fully contoured shoe sole design of the applicant's prior invention that follows the natural contour of all of the foot, the bottom as well as the sides, while retaining a constant shoe sole thickness in the frontal plane.

The fully contoured shoe sole assumes that the resulting slightly rounded bottom when unloaded will deform under load and flatten lust as the human foot bottom is slightly rounded unloaded but flattens under load; therefore, shoe sole material must be of such composition as to allow the natural deformation following that of the foot. The design applies particularly to the heel, but to the rest of the shoe sole as well. By providing the closest match to the natural shape of the foot, the fully contoured design allows the foot to function as naturally as possible. Under load, FIG. **2** would deform by flattening to look essentially like FIG. **24**. Seen in this light, the naturally contoured side design in FIG. **24** is a more conventional, conservative design that is a special case of the more general fully contoured design in FIG. **25**, which is the closest to the natural form of the foot, but the least conventional. The amount of deformation flattening

used in the FIG. 24 design, which obviously varies under different loads, is not an essential element of the applicant's invention.

FIGS. 24 and 25 both show in frontal plane cross sections the essential concept underlying this invention, the theoretically ideal stability plane, which is also theoretically ideal for efficient natural motion of all kinds, including running, jogging or walking. FIG. 25 shows the most general case of the invention, the fully contoured design, which conforms to the natural shape of the unloaded foot. For any given individual, the theoretically ideal stability plane 51 is determined, first, by the desired shoe sole thickness(es) in a frontal plane cross section, and, second, by the natural shape of the individual's foot surface 29.

For the special case shown in FIG. 24, the theoretically ideal stability plane for any particular individual (or size average of individuals) is determined, first, by the given frontal plane cross section shoe sole thickness(es); second, by the natural shape of the individual's foot; and, third, by the frontal plane cross section width of the individual's load-bearing footprint 30b, which is defined as the upper surface of the shoe sole that is in physical contact with and supports the human foot sole.

The theoretically ideal stability plane for the special case is composed conceptually of two parts. Shown in FIG. 24, the first part is a line segment 31b of equal length and parallel to line 30b at a constant distance(s) equal to shoe sole thickness. This corresponds to a conventional shoe sole directly underneath the human foot, and also corresponds to the flattened portion of the bottom of the load-bearing foot sole 28b. The second part is the naturally contoured stability side outer edge 31a located at each side of the first part, line segment 31b. Each point on the contoured side outer edge 31a is located at a distance which is exactly shoe sole thickness(es) from the closest point on the contoured side inner edge 30a.

In summary, the theoretically ideal stability plane is the essence of this invention because it is used to determine a geometrically precise bottom contour of the shoe sole based on a top contour that conforms to the contour of the foot. This invention specifically claims the exactly determined geometric relationship just described.

It can be stated unequivocally that any shoe sole contour, even of similar contour, that exceeds the theoretically ideal stability plane will restrict natural foot motion, while any less than that plane will degrade natural stability, in direct proportion to the amount of the deviation. The theoretical ideal was taken to be that which is closest to natural.

FIG. 26 illustrates in frontal plane cross section another variation of the applicant's prior invention that uses stabilizing quadrants 26 at the outer edge of a conventional shoe sole 28b illustrated Generally at the reference numeral 28. The stabilizing quadrants would be abbreviated in actual embodiments.

FIG. 27 [6] shows a thickness variation which is symmetrical as in the case of FIGS. 4 and 5, but wherein the shoe sole begins to thicken beyond the theoretically ideal stability plane 51 directly underneath the foot heel 27 on about a center line of the shoe sole. In fact, in this case the thickness of the shoe sole is the same as the theoretically ideal stability plane only at that beginning point underneath the upright foot. For the applicant's new invention where the shoe sole thickness varies, the theoretically ideal stability plane is determined by the least thickness in the shoe sole's direct load-bearing portion meaning that portion with direct tread contact on the ground; the outer edge or periphery of the shoe sole is obviously excluded, since the thickness there

always decreases to zero. Note that the capability to deform naturally of the applicant's design may make some portions of the shoe sole load-bearing when they are actually under a load, especially walking or running, even though they might not appear to be when not under a load.

FIG. 28 [7] shows that the thickness can also increase and then decrease; other thickness variation sequences are also possible. The variation in side contour thickness in the new invention can be either symmetrical on both sides or asymmetrical, particularly with the medial side providing more stability than the lateral side, although many other asymmetrical variations are possible, and the pattern of the right foot can vary from that of the left foot.

FIGS. 29, 30, 6 and 32 [8, 9, 10 & 12] show that similar variations in shoe midsole (other portions of the shoe sole area not shown) density can provide similar but reduced effects to the variations in shoe sole thickness described previously in FIGS. 4, 5, 27 and 28. The major advantage of this approach is that the structural theoretically ideal stability plane is retained, so that naturally optimal stability and efficient motion are retained to the maximum extent possible.

The forms of dual and tri-density midsoles shown in the figures are extremely common in the current art of running shoes, and any number of densities are theoretically possible, although an angled alternation of just two densities like that shown in FIG. 29 provides continually changing composite density. However, the applicant's prior invention did not prefer multi-densities in the midsole, since only a uniform density provides a neutral shoe sole design that does not interfere with natural foot and ankle biomechanics in the way that multi-density shoe soles do, which is by providing different amounts of support to different parts of the foot; it did not, of course, preclude such multi-density midsoles. In these figures, the density of the sole material designated by the legend (d1) is firmer than (d) while (d2) is the firmest of the three representative densities shown. In FIG. 29, a dual density sole is shown, with (d) having the less firm density.

It should be noted that shoe soles using a combination both of sole thicknesses greater than the theoretically ideal stability plane and of midsole densities variations like those just described are also possible but not shown.

In particular, it is anticipated that individuals with overly rigid feet, those with restricted range of motion, and those tending to over-supinate may benefit from the FIG. 33 embodiments. Even more particularly, it is expected that the invention will benefit individuals with significant bilateral foot function asymmetry: namely, a tendency toward pronation on one foot and supination on the other foot. Consequently, it is anticipated that this embodiment would be used only on the shoe sole of the supinating foot, and on the inside portion only, possibly only a portion thereof. It is expected that the range less than the theoretically ideal stability plane would be a maximum of about five to ten percent, though a maximum of up to twenty-five percent may be beneficial to some individuals.

FIG. 33A [14] shows an embodiment like FIGS. 4 and 28, but with naturally contoured sides less than the theoretically ideal stability plane. FIG. 33B shows an embodiment like the fully contoured design in FIGS. 5 and 6, but with a shoe sole thickness decreasing with increasing distance from the center portion of the sole. FIG. 33C shows an embodiment like the quadrant-sided design of FIG. 31, but with the quadrant sides increasingly reduced from the theoretically ideal stability plane.

The lesser-sided design of FIG. 33 would also apply to the FIGS. 29, 30, 6 and 32 density variation approach and to the FIG. 8 approach using tread design to approximate density variation.

FIG. 34 A–C [15] show, in cross sections similar to those in pending U.S. Pat. No. '349, that with the quadrant-sided design of FIGS. 26, 31, 32 and 33C that it is possible to have shoe sole sides that are both greater and lesser than the theoretically ideal stability plane in the same shoe. The radius of an intermediate shoe sole thickness, taken at (S²) at the base of the fifth metatarsal in FIG. 34B, is maintained constant throughout the quadrant sides of the shoe sole, including both the heel, FIG. 34C, and the forefoot, FIG. 34A, so that the side thickness is less than the theoretically ideal stability plane at the heel and more at the forefoot. Though possible, this is not a preferred approach.

The same approach can be applied to the naturally contoured sides or fully contoured designs described in FIGS. 24, 25, 4, 5, 6, 8, and 27–30, but it is also not preferred. In addition, is shown in FIGS. 34D–F, in cross sections similar to those in pending U.S. application Ser. No. 07/239,667, it is possible to have shoe sole sides that are both greater and lesser than the theoretically ideal stability plane in the same shoe, like FIGS. 34A–C, but wherein the side thickness (or radius) is neither constant like FIGS. 34A–C or varying directly with shoe sole thickness, like in the applicant's pending applications, but instead varying quite indirectly with shoe sole thickness. As shown in FIGS. 34D–F, the shoe sole side thickness varies from somewhat less than shoe sole thickness at the heel to somewhat more at the forefoot. This approach, though possible, is again not preferred, and can be applied to the quadrant sided design, but is not preferred there either.

FIG. 35 [1] shows a perspective view of a shoe, such as a typical athletic shoe specifically for running, according to the prior art, wherein the running shoe 20 includes an upper portion 21 and a sole 22.

FIG. 36 [2] illustrates, in a close-up cross section of a typical shoe of existing art (undeformed by body weight) on the around 43 when tilted on the bottom outside edge 23 of the shoe sole 22, that an inherent stability problem remains in existing designs, even when the abnormal torque producing rigid heel counter and other motion devices are removed, as illustrated in FIG. 5 of pending U.S. application Ser. No. 07/400,714, filed on Aug. 30, 1989, shown as FIG. 16 in this application. The problem is that the remaining shoe user 21 (shown in the thickened and darkened line), while providing no lever arm extension, since it is flexible instead of rigid, nonetheless creates unnatural destabilizing torque on the shoe sole. The torque is due to the tension force 155a along the top surface of the shoe sole 22 caused by a compression force 150 (a composite of the force of gravity on the body and a sideways motion force) to the side by the foot 27, due simply to the shoe being tilted to the side, for example. The resulting destabilizing force acts to pull the shoe sole in rotation around a lever arm 23a that is the width of the shoe sole at the edge. Roughly speaking, the force of the foot on the shoe upper pulls the shoe over on its side when the shoe is tilted sideways. The compression force 150 also creates a tension force 155b, which is the mirror image of tension force 155a

FIG. 37 [3] shows, in a close-up cross section of a naturally contoured design shoe sole 28, described in pending U.S. application Ser. No. 07/239,667, filed on Sep. 2, 1988, (also shown undeformed by body weight) when tilted on the bottom edge, that the same inherent stability problem remains in the naturally contoured shoe sole design, though

to a reduced degree. The problem is less since the direction of the force vector 155 along the lower surface of the shoe upper 21 is parallel to the ground 43 at the outer sole edge 32 edge, instead of angled toward the around as in a conventional design like that shown in FIG. 36, so the resulting torque produced by lever arm created by the outer sole edge 32 would be less, and the contoured shoe sole 28 provides direct structural support when tilted, unlike conventional designs.

FIG. 38 [4] shows (in a rear view) that, in contrast, the barefoot is naturally stable because, when deformed by body weight and tilted to its natural lateral limit of about 20 degrees, it does not create any destabilizing torque due to tension force. Even though tension paralleling that on the shoe upper is created on the outer surface 29, both bottom and sides, of the bare foot by the compression force of weight-bearing, no destabilizing torque is created because the lower surface under tension (ie the foot's bottom sole, shown in the darkened line) is resting directly in contact with the ground. Consequently, there is no unnatural lever arm artificially created against which to pull. The weight of the body firmly anchors the outer surface of the foot underneath the foot so that even considerable pressure against the outer surface 29 of the side of the foot results in no destabilizing motion. When the foot is tilted, the supporting structures of the foot, like the calcaneus, slide against the side of the strong but flexible outer surface of the foot and create very substantial pressure on that outer surface at the sides of the foot. But that pressure is precisely resisted and balanced by tension along the outer surface of the foot, resulting in a stable equilibrium.

FIG. 39 [5] shows, in cross section of the upright heel deformed by body weight, the principle of the tension stabilized sides of the barefoot applied to the naturally contoured shoe sole design; the same principle can be applied to conventional shoes, but is not shown. The key chance from the existing art of shoes is that the sides of the shoe upper 21 (shown as darkened lines) must wrap around the outside edges 32 of the shoe sole 28, instead of attaching underneath the foot to the upper surface 30 of the shoe sole, as done conventionally. The shoe upper sides can overlap and be attached to either the inner (shown on the left) or outer surface (shown on the right) of the bottom sole, since those sides are not unusually load-bearing, as shown; or the bottom sole, optimally thin and tapering as shown, can extend upward around the outside edges 32 of the shoe sole to overlap and attach to the shoe upper sides (shown FIG. 39B); their optimal position coincides with the Theoretically Ideal Stability Plane, so that the tension force on the shoe sides is transmitted directly all the way down to the bottom shoe, which anchors it on the around with virtually no intervening artificial lever arm. For shoes with only one sole layer, the attachment of the shoe upper sides should be at or near the lower or bottom surface of the shoe sole.

The design shown in FIG. 39 is based on a fundamentally different conception: that the shoe upper is integrated into the shoe sole, instead of attached on top of it, and the shoe sole is treated as a natural extension of the foot sole, not attached to it separately.

The fabric (or other flexible material, like leather) of the shoe uppers would preferably be non-stretch or relatively so, so as not to be deformed excessively by the tension place upon its sides when compressed as the foot and shoe tilt. The fabric can be reinforced in areas of particularly high tension, like the essential structural support and propulsion elements defined in the applicant's earlier applications (the base and lateral tuberosity of the calcaneus, the base of the fifth

metatarsal, the heads of the metatarsals, and the first distal phalange; the reinforcement can take many forms, such as like that of corners of the jib sail of a racing sailboat or more simple straps. As closely as possible, it should have the same performance characteristics as the heavily calloused skin of the sole of an habitually bare foot. The relative density of the shoe sole is preferred as indicated in FIG. 9 of pending U.S. application Ser. No. 07/400,714, filed on Aug. 30, 1989, with the softest density nearest the foot sole, so that the conforming sides of the shoe sole do not provide a rigid destabilizing lever arm.

The change from existing art of the tension stabilized sides shown in FIG. 39 is that the shoe upper is directly integrated functionally with the shoe sole, instead of simply being attached on top of it. The advantage of the tension stabilized sides design is that it provides natural stability as close to that of the barefoot as possible, and does so economically, with the minimum shoe sole side width possible.

The result is a shoe sole that is naturally stabilized in the same way that the barefoot is stabilized, as seen in FIG. 40 [6], which shows a close-up cross section of a naturally contoured design shoe sole 28 (undeformed by body weight) when tilted to the edge. The same destabilizing force against the side of the shoe shown in FIG. 36 is now stably resisted by offsetting tension in the surface of the shoe upper 21 extended down the side of the shoe sole so that it is anchored by the weight of the body when the shoe and foot are tilted.

In order to avoid creating unnatural torque on the shoe sole, the shoe uppers may be joined or bonded only to the bottom sole, not the midsole, so that pressure shown on the side of the shoe upper produces side tension only and not the destabilizing torque from pulling similar to that described in FIG. 36. However, to avoid unnatural torque, the upper areas 147 of the shoe midsole, which forms a sharp corner, should be composed of relatively soft midsole material; in this case, bonding the shoe uppers to the midsole would not create very much destabilizing torque. The bottom sole is preferably thin, at least on the stability sides, so that its attachment overlap with the shoe upper sides coincide as close as possible to the Theoretically Ideal Stability Plane, so that force is transmitted on the outer shoe sole surface to the ground.

In summary, the FIG. 39 design is for a shoe construction, including: a shoe upper that is composed of material that is flexible and relatively inelastic at least where the shoe upper contacts the areas of the structural bone elements of the human foot, and a shoe sole that has relatively flexible sides; and at least a portion of the sides of the shoe upper being attached directly to the bottom sole, while enveloping on the outside the other sole portions of said shoe sole. This construction can either be applied to convention shoe sole structures or to the applicant's prior shoe sole inventions, such as the naturally contoured shoe sole conforming to the theoretically ideal stability plane.

FIG. 41 [7] shows, in cross section at the heel, the tension stabilized sides concept applied to naturally contoured design shoe sole when the shoe and foot are tilted out fully and naturally deformed by body weight (although constant shoe sole thickness is shown undeformed). The figure shows that the shape and stability function of the shoe sole and shoe uppers mirror almost exactly that of the human foot.

FIGS. 42A–42D [8] show the natural cushioning of the human barefoot, in cross sections at the heel. FIG. 42A shows the bare heel upright and unloaded, with little pressure on the subcalcaneal fat pad 158, which is evenly distributed between the calcaneus 159, which is the heel bone, and the bottom sole 160 of the foot.

FIG. 42B shows the bare heel upright but under the moderate pressure of full body weight. The compression of the calcaneus against the subcalcaneal fat pad produces evenly balanced pressure within the subcalcaneal fat pad because it is contained and surrounded by a relatively unstretchable fibrous capsule, the bottom sole of the foot. Underneath the foot, where the bottom sole is in direct contact with the ground, the pressure caused by the calcaneus on the compressed subcalcaneal fat pad is transmitted directly to the ground. Simultaneously, substantial tension is created on the sides of the bottom sole of the foot because of the surrounding relatively tough fibrous capsule. That combination of bottom pressure and side tension is the foot's natural shock absorption system for support structures like the calcaneus and the other bones of the foot-that come in contact with the ground.

Of equal functional importance is that lower surface 167 of those support structures of the foot like the calcaneus and other bones make firm contact with the upper surface 168 of the foot's bottom sole underneath, with relatively little uncompressed fat pad intervening. In effect, the support structures of the foot land on the around and are firmly supported; they are not suspended on top of springy material in a buoyant manner analogous to a water bed or pneumatic tire, like the existing proprietary shoe sole cushioning systems like Nike Air or Asics Gel. This simultaneously firm and yet cushioned support provided by the foot sole must have a significantly beneficial impact on energy efficiency, also called energy return, and is not paralleled by existing shoe designs to provide cushioning, all of which provide shock absorption cushioning during the landing and support phases of locomotion at the expense of firm support during the take-off phase.

The incredible and unique feature of the foot's natural system is that, once the calcaneus is in fairly direct contact with the bottom sole and therefore providing firm support and stability, increased pressure produces a more rigid fibrous capsule that protects the calcaneus and greater tension at the sides to absorb shock. So, in a sense, even when the foot's suspension system would seem in a conventional way to have bottomed out under normal body weight pressure, it continues to react with a mechanism to protect and cushion the foot even under very much more extreme pressure. This is seen in FIG. 42C, which shows the human heel under the heavy pressure of roughly three times body weight force of landing during routine running. This can be easily verified: when one stands barefoot on a hard floor, the heel feels very firmly supported and vet can be lifted and virtually slammed onto the floor with little increase in the feeling of firmness; the heel simply becomes harder as the pressure increases.

In addition, it should be noted that this system allows the relatively narrow base of the calcaneus to pivot from side to side freely in normal pronation/supination motion, without any obstructing torsion on it, despite the very much greater width of compressed foot sole providing protection and cushioning; this is crucially important in maintaining natural alignment of joints above the ankle joint such as the knee, hip and back, particularly in the horizontal plane, so that the entire body is properly adjusted to absorb shock correctly. In contrast, existing shoe sole designs, which are generally relatively wide to provide stability, produce unnatural frontal plane torsion on the calcaneus, restricting its natural motion, and causing misalignment of the joints operating above it, resulting in the overuse injuries unusually common

with such shoes. Instead of flexible sides that harden under tension caused by pressure like that of the foot, existing shoe sole designs are forced by lack of other alternatives to use relatively rigid sides in an attempt to provide sufficient stability to offset the otherwise uncontrollable buoyancy and lack of firm support of air or gel cushions.

FIG. **42**D shows the barefoot deformed under full body weight and tilted laterally to the roughly 20 degree limit of normal range. Again it is clear that the natural system provides both firm lateral support and stability by providing relatively direct contact with the ground, while at the same time providing a cushioning mechanism through side tension and subcalcaneal fat pad pressure.

FIGS. **43**A–D show FIGS. 9B–D of the '302 application, in addition to FIG. **9** of this application.

While the FIG. **9** and FIG. **43** design copies in a simplified way the macro structure of the foot. FIGS. **44** [10] A–C focus on a more on the exact detail of the natural structures, including at the micro level. FIGS. **44**A and **44**C are Perspective views of cross sections of the human heel showing the matrix of elastic fibrous connective tissue arranged into chambers **164** holding closely packed fat cells; the chambers are structured as whorls radiating out from the calcaneus. These fibrous-tissue strands are firmly attached to the undersurface of the calcaneus and extend to the subcutaneous tissues. They are usually in the form of the letter U, with the open end of the U pointing toward the calcaneus.

As the most natural, an approximation of this specific chamber structure would appear to be the most optimal as an accurate model for the structure of the shoe sole cushioning compartments **161**, at least in an ultimate sense, although the complicated nature of the design will require some time to overcome exact design and construction difficulties; however, the description of the structure of calcaneal padding provided by Erich Blechschmidt in Foot and Ankle, March, 1982, (translated from the original 1933 article in German) is so detailed and comprehensive that copying the same structure as a model in shoe sole design is not difficult technically, once the crucial connection is made that such copying of this natural system is necessary to overcome inherent weaknesses in the design of existing shoes. Other arrangements and orientations of the whorls are possible, but would probably be less optimal.

Pursuing this nearly exact design analogy, the lower surface **165** of the upper midsole **147** would correspond to the outer surface **167** of the calcaneus **159** and would be the origin of the U shaped whorl chambers **164** noted above.

FIG. **44**B shows a close-up of the interior structure of the large chambers shown in FIGS. **44**A and **44**C. It is clear from the fine interior structure and compression characteristics of the mini-chambers **165** that those directly under the calcaneus become very hard quite easily, due to the high local pressure on them and the limited degree of their elasticity, so they are able to provide very firm support to the calcaneus or other bones of the foot sole; by being fairly inelastic, the compression forces on those compartments are dissipated to other areas of the network of fat pads under any given support structure of the foot, like the calcaneus. Consequently, if a cushioning compartment **161**, such as the compartment under the heel shown in FIGS. **9** & **43**, is subdivided into smaller chambers, like those shown in FIG. **44**, then actual contact between the upper surface **165** and the lower surface **166** would no longer be required to provide firm support, so long as those compartments and the pressure-transmitting medium contained in them have material characteristics similar to those of the foot, as described

above; the use of gas may not be satisfactory in this approach, since its compressibility may not allow adequate firmness.

In summary, the FIG. **44** design shows a shoe construction including: a shoe sole with a compartments under the structural elements of the human foot, including at least the heel; the compartments containing a pressure-transmitting medium like liquid, gas, or gel; the compartments having a whorled structure like that of the fat pads of the human foot sole; load-bearing pressure being transmitted progressively at least in part to the relatively inelastic sides, ton and bottom of the shoe sole compartments, producing tension therein; the elasticity of the material of the compartments and the pressure-transmitting medium are such that normal weight-bearing loads produce sufficient tension within the structure of the compartments to provide adequate structural rigidity to allow firm natural support to the foot structural elements, like that provided the barefoot by its fat pads. That shoe sole construction can have shoe sole compartments that are subdivided into micro chambers like those of the fat pads of the foot sole.

Since the bare foot that is never shod is protected by very hard callouses (called a "seri boot") which the shod foot lacks, it seems reasonable to infer that natural protection and shock absorption system of the shod foot is adversely affected by its unnaturally undeveloped fibrous capsules (surrounding the subcalcaneal and other fat lads under foot bone support structures). A solution would be to produce a shoe intended for use without socks (ie with smooth surfaces above the foot bottom sole) that uses insoles that coincide with the foot bottom sole, including its sides. The upper surface of those insoles, which would be in contact with the bottom sole of the foot (and its sides), would be coarse enough to stimulate the production of natural barefoot callouses. The insoles would be removable and available in different uniform trades of coarseness, as is sandpaper, so that the user can progress from finer grades to coarser trades as his foot soles toughen with use.

Similarly, socks could be produced to serve the same function, with the area of the sock that corresponds to the foot is bottom sole (and sides of the bottom sole) made of a material coarse enough to stimulate the production of callouses on the bottom sole of the foot, with different grades of coarseness available, from fine to coarse, corresponding to feet from soft to naturally tough. Using a tube sock design with uniform coarseness, rather than conventional sock design assumed above, would allow the user to rotate the sock on his foot to eliminate any "hot spot" irritation points that might develop. Also, since the toes are most crone to blistering and the heel is most important in shock absorption, the toe area of the sock could be relatively less abrasive than the heel area.

Thus, it will clearly be understood by those skilled in the art that the foregoing description has been made in terms of the preferred embodiment and various changes and modifications may be made without departing from the scope of the present invention which is to be defined by the appended claims.

What is claimed is:

1. An athletic shoe sole for supporting a foot of an intended wearer, the shoe sole comprising:

a sole inner surface;

a sole outer surface;

the sole surfaces of the athletic shoe together defining a sole medial side, a sole lateral side, and a sole middle portion between the sole sides;

the sole having a heel portion at a location substantially corresponding to a heel of the intended wearer's foot, a forefoot portion at a location substantially corresponding to a forefoot of the intended wearer's foot, and a third portion between the heel and forefoot portions;

the heel portion having a lateral heel part at a location substantially corresponding to the lateral tuberosity of the calcaneus of the intended wearer's foot, and a medial heel part at a location substantially corresponding to the base of the calcaneus of the intended wearer's foot;

the third portion having a lateral midtarsal part at a location substantially corresponding to the base of a fifth metatarsal of the intended wearer's foot, and a main longitudinal arch part at a location substantially corresponding to the longitudinal arch of the intended wearer's foot;

the forefoot portion having a forward medial forefoot part at a location substantially corresponding to the head of the first distal phalange of the intended wearer's foot, and rear medial and lateral forefoot parts at locations substantially corresponding to the heads of the medial and lateral metatarsals of the intended wearer's foot;

an outer sole;

at least two rounded portions, each formed by midsole component, each said rounded midsole portion being located between a convexly rounded portion of an inner surface of the midsole component and a concavely rounded portion of an outer surface of the midsole component, as viewed in a shoe sole frontal plane cross-section when the shoe sole is upright and in an unloaded condition, the convexity of the convexly rounded portion of the inner surface of the midsole component existing with respect to a section of the midsole component located adjacent to the convexly rounded inner surface portion, and the concavity of the concavely rounded portion of the outer surface of the midsole component existing with respect to an inner section of the midsole component located adjacent to the concavely rounded outer surface portion;

each of said rounded midsole portions being located at a different position on the sole, the different positions comprising positions near to at least one of the medial heel part, lateral heel part, forward medial forefoot part, rear medial forefoot part, rear lateral forefoot part, lateral midtarsal part, and main longitudinal arch part;

wherein each of said rounded midsole portions of the shoe sole has a substantially uniform thickness extending from a location proximate to a sidemost extent of the shoe sole side to a lowest point on said sole side, as viewed in a frontal plane cross-section when the shoe sole is upright and in an unloaded condition;

at least two tapered portions having a thickness that decreases gradually from a first thickness to a lesser thickness, as viewed in a shoe sole horizontal plane when the shoe sole is upright and in an unloaded condition, said thickness of each of said tapered portions being measured from the inner surface of the midsole component to the outer surface of the shoe sole, and each of said tapered portions being located at a location on the shoe sole corresponding to a location of each of the rounded midsole portions;

the sole having a lateral sidemost section being located at a location outside of a straight vertical line extending through the shoe sole at a lateral sidemost extent of the inner surface of the midsole component, as viewed in a shoe sole frontal plane cross-section when the shoe sole is upright and in an unloaded condition;

the sole having a medial sidemost section being located at a location outside of a straight vertical line extending through the shoe sole at a medial sidemost extent of the inner surface of the midsole component, as viewed in a shoe sole frontal plane cross-section when the shoe sole is upright and in an unloaded condition;

a midsole part extends into the sidemost section of the sole side at the location of each of said rounded midsole portions, as viewed in a shoe sole frontal plane cross-section when the shoe sole is upright and in an unloaded condition;

each said midsole part further extends to above a level corresponding to the lowest point of the midsole component inner surface of the same sole side, as viewed in a shoe sole frontal plane cross-section when the shoe sole is upright and in an unloaded condition; and

said shoe sole has a heel portion thickness that is greater than a forefoot portion thickness, as viewed in a shoe sole sagittal plane cross-section when the shoe sole is upright and in an unloaded condition.

2. The shoe sole of claim 1, wherein the shoe sole comprises at least three said rounded midsole portions.

3. The shoe sole of claim 1, wherein the shoe sole comprises at least four said rounded midsole portions.

4. The shoe sole of claim 1, wherein the shoe sole comprises at least five said rounded midsole portions.

5. The shoe sole of claim 1, wherein the shoe sole comprises at least six said rounded midsole portions.

6. The shoe sole of claim 1, wherein the shoe sole comprises at least seven said rounded midsole portions.

7. The shoe sole of claim 1, wherein one said rounded midsole portion is located at the lateral midtarsal part.

8. The shoe sole of claim 1, wherein one said rounded midsole portion is located at the main longitudinal arch part.

9. The shoe sole of claim 1, wherein one said rounded midsole portion is located at the medial heel part.

10. The shoe sole of claim 1, wherein one said rounded midsole portion is located at the rear medial forefoot part.

11. The shoe sole of claim 1, wherein one said rounded midsole portion is located at the rear lateral forefoot part.

12. The shoe sole of claim 1, wherein one rounded midsole portion is located at the lateral heel part.

13. The shoe sole of claim 1, wherein one said rounded midsole portion is located at the forward medial forefoot part.

14. The shoe sole of claim 1, comprising at least three rounded midsole portions, each of which rounded midsole portions is located in the forefoot portion of the shoe sole.

15. The shoe sole of claim 1, wherein said at least two rounded midsole portions are located at the rear medial forefoot part and the rear lateral forefoot part.

16. The shoe sole of claim 1, wherein said at least two rounded midsole portions are located at the rear medial forefoot part and the forward medial forefoot part.

17. The shoe sole of claim 1, wherein at least part of the outer surface of each said tapered portion is concavely rounded, as viewed in the shoe sole horizontal plane when the shoe sole is upright and in an unloaded condition, the concavity existing with respect to an inner section of the shoe sole located adjacent to the concavely rounded outer surface of the tapered portion of the shoe sole.

18. The shoe sole of claim 1, wherein the shoe sole further comprises, at the location of each said rounded midsole portion, a second tapered portion having a thickness that decreases gradually from a first thickness to a lesser thick-

ness, as viewed in a shoe sole horizontal plane when the shoe sole is upright and in an unloaded condition.

19. The shoe sole of claim 18, wherein at least part of the outer surface of each said second tapered portion is concavely rounded, the concavity being determined relative to an inner section of the tapered portion adjacent to the concavely rounded outer surface portion of each said second tapered portion, as viewed in a shoe sole horizontal plane when the shoe sole is upright and in an unloaded condition.

20. An athletic shoe sole for supporting a foot of an intended wearer, the shoe sole comprising:

a sole inner surface;

a sole outer surface;

the sole surfaces of the athletic shoe together defining a sole medial side, a sole lateral side, and a sole middle portion between the sole sides;

the sole having a heel portion at a location substantially corresponding to a heel of the intended wearer's foot, a forefoot portion at a location substantially corresponding to a forefoot of the intended wearer's foot, and a third portion between the heel and forefoot portions;

the heel portion having a lateral heel part at a location substantially corresponding to the lateral tuberosity of the calcaneus of the intended wearer's foot, and a medial heel part at a location substantially corresponding to the base of the calcaneus of the intended wearer's foot;

the third portion having a lateral midtarsal part at a location substantially corresponding to the base of a fifth metatarsal of the intended wearer's foot, and a main longitudinal arch part at a location substantially corresponding to the longitudinal arch of the intended wearer's foot;

the forefoot portion having a forward medial forefoot part at a location substantially corresponding to the head of the first distal phalange of the intended wearer's foot, and rear medial and lateral forefoot parts at locations substantially corresponding to the heads of the medial and lateral metatarsals of the intended wearer's foot;

an outer sole;

at least two rounded portions, each formed by midsole component, each said rounded midsole portion being located between a convexly rounded portion of an inner surface of the midsole component and a concavely rounded portion of an outer surface of the midsole component, as viewed in a shoe sole frontal plane cross-section when the shoe sole is upright and in an unloaded condition, the convexity of the convexly rounded portion of the inner surface of the midsole component existing with respect to a section of the midsole component located adjacent to the convexly rounded inner surface portion, and the concavity of the concavely rounded portion of the outer surface of the midsole component existing with respect to an inner section of the midsole component located adjacent to the concavely rounded outer surface portion;

each of said rounded midsole portions being located at a different position on the sole, the different positions comprising positions near to at least one of the medial heel part, lateral heel part, forward medial forefoot part, rear medial forefoot part, rear lateral forefoot part, lateral midtarsal part, and main longitudinal arch part;

wherein each of said rounded midsole portions of the shoe sole has a substantially uniform thickness extending from a height of a lowest point of the inner surface of the midsole component to a lowest point on said sole

side, as viewed in a frontal plane cross-section when the shoe sole is upright and in an unloaded condition;

at least two tapered portions having a thickness that decreases gradually from a first thickness to a lesser thickness, as viewed in a shoe sole horizontal plane when the shoe sole is upright and in an unloaded condition, said thickness of each of said tapered portions being measured from the inner surface of the midsole component to the outer surface of the shoe sole, and each of said tapered portions being located at a location on the shoe sole corresponding to a location of each of the rounded midsole portions;

the sole having a lateral sidemost section being located at a location outside of a straight vertical line extending through the shoe sole at a lateral sidemost extent of the inner surface of the midsole component, as viewed in a shoe sole frontal plane cross-section when the shoe sole is upright and in an unloaded condition;

the sole having a medial sidemost section being located at a location outside of a straight vertical line extending through the shoe sole at a medial sidemost extent of the inner surface of the midsole component, as viewed in a shoe sole frontal plane cross-section when the shoe sole is upright and in an unloaded condition;

a midsole part extends into the sidemost section of the sole side at the location of each of said rounded midsole portions, as viewed in a shoe sole frontal plane cross-section when the shoe sole is upright and in an unloaded condition;

each said midsole part further extends to above a level corresponding to the lowest point of the midsole component inner surface of the same sole side, as viewed in a shoe sole frontal plane cross-section when the shoe sole is upright and in an unloaded condition; and

said shoe sole has a heel portion thickness that is greater than a forefoot portion thickness, as viewed in a shoe sole sagittal plane cross-section when the shoe sole is upright and in an unloaded condition.

21. An athletic shoe sole for supporting a foot of an intended wearer, the shoe sole comprising:

a sole inner surface;

a sole outer surface;

the sole surfaces of the athletic shoe together defining a sole medial side, a sole lateral side, and a sole middle portion between the sole sides;

the sole having a heel portion at a location substantially corresponding to a heel of the intended wearer's foot, a forefoot portion at a location substantially corresponding to a forefoot of the intended wearer's foot, and a third portion between the heel and forefoot portions;

the heel portion having a lateral heel part at a location substantially corresponding to the lateral tuberosity of the calcaneus of the intended wearer's foot, and a medial heel part at a location substantially corresponding to the base of the calcaneus of the intended wearer's foot;

the third portion having a lateral midtarsal part at a location substantially corresponding to the base of a fifth metatarsal of the intended wearer's foot, and a main longitudinal arch part at a location substantially corresponding to the longitudinal arch of the intended wearer's foot;

the forefoot portion having a forward medial forefoot part at a location substantially corresponding to the head of the first distal phalange of the intended wearer's foot, and rear medial and lateral forefoot parts at locations

substantially corresponding to the heads of the medial and lateral metatarsals of the intended wearer's foot;

at least two rounded portions, each said rounded portion being located between a convexly rounded portion of an inner surface of the shoe sole and a concavely 5 rounded portion of an outer surface of the shoe sole, as viewed in a shoe sole frontal plane cross-section when the shoe sole is upright and in an unloaded condition, the convexity of the convexly rounded portion of the inner surface of the shoe sole existing with respect to a 10 section of the shoe sole located adjacent to the convexly rounded inner surface portion, and the concavity of the concavely rounded portion of the outer surface of the shoe sole existing with respect to an inner section of the shoe sole located adjacent to the concavely 15 rounded outer surface portion;

each of said rounded portions being located at a different position on the sole, the different positions comprising positions near to at least one of the medial heel part, lateral heel part, forward medial forefoot part, rear 20 medial forefoot part, rear lateral forefoot part, lateral midtarsal part, and main longitudinal arch part;

wherein each of said rounded portions of the shoe sole has a substantially uniform thickness extending from a location proximate to a sidemost extent of the shoe sole side to a lowest point on said sole side, as viewed in a frontal plane cross-section when the shoe sole is upright and in an unloaded condition;

at least two tapered portions having a thickness that decreases gradually from a first thickness to a lesser thickness, as viewed in a shoe sole horizontal plane when the shoe sole is upright and in an unloaded condition, said thickness of each of said tapered portions being measured from the inner surface of the shoe sole to the outer surface of the shoe sole, and each of said tapered portions being located at a location on the shoe sole corresponding to a location of each of the rounded portions; and

said shoe sole has a heel portion thickness that is greater than a forefoot portion thickness, as viewed in a shoe sole sagittal plane cross-section when the shoe sole is upright and in an unloaded condition.

* * * * *